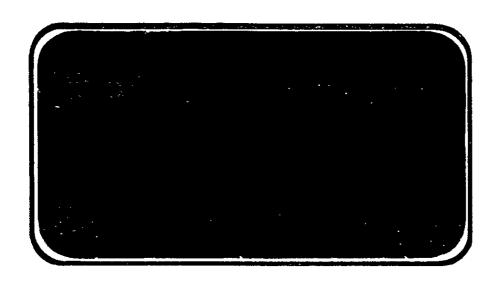


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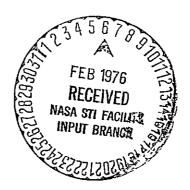
(NASA-CR-141834) RESULTS OF AN INVESTIGATION OF HYPERSONIC VISCOUS INTERACTION EFFECTS OF THE SPACE SHUTTLE ORBITER USING A 0.010 SCALE MODEL (51-0) IN THE AEDC-VKF TUNNEL F (OA160) (Chrysler

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SPACE SHUTTLE

AEROTHERMODYNAMIC DATA REPORT



JOHNSON SPACE CENTER HOUSTON, TEXAS

DATA MANagement services

SPACE DIVISION CHRYSLER

DMS DR-2247

NASA CR-141,834

RESULTS OF AN INVESTIGATION OF HYPERSONIC VISCOUS INTERACTION EFFECTS OF THE SPACE SHUTTLE ORBITER USING A 0.010 SCALE MODEL (51-0) IN THE AEDC-VKF TUNNEL F (\$\phi\$a160)

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Prepared under NASA Contract Number NAS9-13247

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for

Engineering Analysis Division

Johnson Space Center National Aeronautics and Space Administration Houston, Texas

WIND TUNNEL TEST SPECIFICS:

Test Number: AEDC VKF V41F-28A

NASA Series Number: OA160 Model Number: 51-0

Test Dates: February 5 through February 11, 1975

Occupancy Hours: 12

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bу

D. J. Elder, Rockwell International

ABSTRACT

An experimental aerodynamic investigation was conducted in the AEDC-VKF Hypervelocity Wind Tunnel (Tunnel F) at a nominal Mach number of 19 to determine hypersonic viscous interaction effects on the Space Shuttle Orbiter. The tests were conducted at an angle-of-attack of 30 degrees over a free-stream Reynolds number (based on fuselage length) variation from 0.1 to 0.4 million. Viscous interaction parameter $(\overline{V}_{\omega}^{\dagger})$ was varied from 0.02 to 0.06. Six component static stability force and moment data were measured by an internally compensated internal strain gage balance. Resulting data are presented in this report.



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NOMENCLATURE

¢ SYMBOL	PLOT SYMBOL	DEFINITION
		Base area, in ²
Argania bref C _{Af}	BREF	Reference span, 936.7 in.
$\mathtt{c}_{\mathtt{A}_{\mathbf{f}}}$	CAF	Forebody axial force coefficient, $^{\rm C}_{{ m A}_{ m T}}$ - $^{\rm C}_{{ m A}_{ m b}}$
$c_{A_{\overline{b}}}$	CAB ,	Base axial force coefficient, $[(P_{\infty} - P_b)/q_{\infty}] A_b/S_{ref}$
c _{ÅT}	CA	Total axial-force coefficient, $F_{A_{\mathrm{T}}}/q_{\infty} S_{\mathrm{ref}}$
$c_{\tilde{D}}$	CD	Drag force coefficient in the stability axis system, C_{A} cos α - C_{N} sin α
$c_\mathtt{L}$	CL	Lift force coefficient (stability or wind axis), $C_{\rm N}$ cos $\alpha C_{\rm A}$ sin α
C_{m}	CLM	Pitching-moment coefficient about Sta 1076.7, pitching moment/ $q_{\infty}S_{\text{ref}}^{\ell}_{\text{ref}}$
c_N	CN	Normal-force coefficient in the body axis system, $F_{\rm N}/q_{_{\infty}}S_{\rm ref}$
C_{∞}		Chapman Rubensin viscosity coefficient
C _∞ ¹		Viscosity coefficient, see data reduction section
FAT		Total axial force, lb
FAT F		Normal force, 1b
$\mathbf{F_{N}}_{A}$		Normal-force component measured at aft normal-force gage location, 1b
${ m F_{N_F}}$		Normal-force component measured at forward normal-force gage location, 1b
н:		Enthalpy
IML	IML,	Inner Mold Line

NOMENCLATURE (Continued)

SYMBOL	PLOT SYMBOL	DEFINITION
L/D	L/D	Lift-to-drag ratio, $C_{\rm L}/C_{\rm D}$ (stability axis system)
L		Body reference length, 1290.3 in. (actual model body length was 12.875 in.)
^l ref	LREF	Reference chord, 474.8 in.
М	MACH	Free-stream Mach number
MRP	MRP	Moment reference point
OML	OML	Outer mold line
P _b		Model base pressure, psia
Po	P(0)	Reservoir pressure, psi
P ₀	PITOT	Total pressure behind normal shock in test section, psia
P_{∞}	P	Free-stream static pressure, psia x 10 in Tabulated Data Listing
ф́о	QDOT	Stagnation heat-transfer rate on 1.0 indiam probe, Btu/ft ² -sec
q_{∞}	Q(PSI)	Free-stream dynamic pressure, psia
$\mathtt{Re}_{\mathtt{\infty} \ell}$	RN/L	Reynolds number based on free-stream conditions and model length
Re _∞ /ft	RN/FT	Reynolds number based on free-stream conditions and 1-ft length
$s_{ exttt{ref}}$	SREF	Reference area, = 2690.0 ft^2
T_{O}	T(0)	Reservoir temperature, OR
T _w		Model surface temperature, ^o R
T_{∞}	T	Free-stream temperature, OR

NOMENCLATURE (Continued)

SYMBOL	PLOT SYMBOL	DEFINITION
t	TIME	Time, msec
V		Velocity, ft/sec
$U_{\infty}^{^{\mathbf{k}}}$	υ	Free-stream velocity, ft/sec
\overline{V}_{∞}	VBAR	Hypersonic viscous parameter, $M_{\infty}\sqrt{C_{\infty}}/\sqrt{\text{Re}_{\infty\ell}}$
₹,	VĽBAR	Hypersonic viscous parameter, (as defined by NASA/LaRC), $M_{\infty}\sqrt{C_{\infty}^{*}}$ / $\sqrt{Re}_{\infty\ell}$
x_{ep_N}/ℓ	XCP/L	Center-of-pressure location, [0.65 - $(C_m \times \ell_{ref})/(C_N \times \ell)$] measured from inner mold line
XMRP	XMRP	Moment reference point on x-axis XMRP = 8.417 in. from nose, $X_0 = 1076.70$ in.
YMRP	YMRP	Moment reference point on y-axis, YMRP = 0
ZMRP	ZMRP	Moment reference point on z-axis, $ZMRP = 25.0 \text{ in. below } Z = 400, Z_0 = 375 \text{ in.}$
x _o	XO	Longitudinal coordinate of model axis system, in.
Yo	YO	Lateral coordinate of model axis system, in.
Z _o	ZO	Vertical coordinate of model axis system, in.
cr 🛊	ALPHA	Angle-of-attack, deg.
α\$		Sector angle of attack, deg.
β	BETA	Angle of sideslip, deg.
δ		Control surface deflection angle, deg, positive deflections are as follows:
	ELEVON	(δ_e) Elevator, trailing edge down positive
	BDFLAP	($\delta_{ m BF}$) Body flap, trailing edge down positive

NOMENCLATURE (Continued)

SYMBOL	PLOT SYMBOL	DEFINITION
	SPDBRK	(δ_{SB}) Speed brake, deflected out from the vertical stabilizer centerline, SB is the included angle
$\mu_{\overline{W}}$		Viscosity at wall temperature
μ_{∞}	MU	Free-stream viscosity
ρ _∞	RHO	Free-stream density, slugs/ft 3 x 10^6 in Tabulated Data Listing
φ	PHI	Model roll angle, deg.

SUBSCRIPTS

BF	Body flap
Ъ	Base
e	Elevons
o	Reservoir
SB	Speed brake
ref	Reference conditions
W	Model wall conditions
δ	Edge of boundary layer
ω	Free-stream conditions

CONFIGURATIONS INVESTIGATED

The test model was a 0.010-scale representation (model 51-0) of a modified NASA Vehicle 4 Orbiter. The full-scale vehicle has a body length of 1290.3 in. and a wingspan of 936.68 in., which corresponds to a model reference length and wingspan of 12.903 and 9.367 in., respectively. The model actual length was 12.875 inches making it shorter than the full scale vehicle configuration. A sketch of the model indicating the general arrangement and pertinent reference stations and dimensions is shown in Fig. 2. A photograph of the orbiter model is presented in Fig. 3.

The model was designed and fabricated prior to the first tunnel F test series (OA81) by AEDC/VKF with the outside contours and overall dimensions traced from a master model provided by Rockwell International (RI), Huntsville, Alabama. The master model was fabricated in conformance with the line drawings as follows:

Nose	VL70-000143A
Mid-body and wing	VL70-000200
Aft body	VL70-000145
Vertical tail	VL70-000146A

The model was constructed of magnesium with all components hollowed or milled out where possible to reduce the overall weight. The upper surfaces of the wings were milled out and filled with foam with an epoxy coating. The model weighed approximately 1.8 lbm. Slight modifications to the outside contours of this model were made under the

direction of RI, prior to the present test series (OA160) and according to the revised model dimensional data dated April 24, 1974.

The wings were equipped with positionable elevons with deflèction angles obtained by exchanging angle plates machined to the desired angles. The elevon deflection angles used were $\delta_{\rm e}$ = -40, 0, and 15 deg with the extremes representing the limits of elevon travel for this configuration. Both the right and left elevons were split approximately midway of each span to represent the full-scale vehicle. However, all elevon surfaces for this test were deployed at the same deflection angle for any given run. The elevon slits were added after the model was installed in the tunnel. A positionable body flap was provided by interchanging separate flaps machined to the proper deflection angles. Body flap angles used were $\delta_{\rm BF}$ = -11.7, 0, and 16.3 deg. The vertical stabilizer component had a fixed rudder and speed brake. Interchangeable stabilizers were available with speed brake deflection angles ($\delta_{\rm SB}$) of 0 and 55 deg. However, only the stabilizer with $\delta_{\rm SB}$ = 0 was used during this test series.

Model components were designated as:

B26	Orbiter body
С9	Canopy
E26	Elevon
F7	Body flap
M7	OMS pods
· N28	OMS nozzle

R5 Rudder

V8 Vertical tail

W116 Wing

Table III provides detailed model dimensional da $% \left\{ \left\{ 1\right\} \right\} =\left\{ 1\right\} =\left\{$

INSTRUMENTATION

The aerodynamic forces were measured with a six-component force balance developed by AEDC/VKF for use in hotshot-type tunnels (Refs. 1 and 2). The balance load cells were instrumented with semiconductor strain gages, and semiconductor accelerometers provided compensation for model inertial loads that result from vibrations of the model and its support hardware. Tunnel F balances are now operated with constant current excitation. This type of excitation in combination with the characteristics of the semiconductor strain gages makes possible a compensation of the balance bridges so that the sensitivities are not affected significantly by changes in temperature. The result is an improvement in calibration accuracy and stability.

The balance used during the test series was calibrated before and after its use in the tunnel. The following uncertainties represent residuals which are differences between combined axial—and normal—force loads applied statically in the calibration laboratory and the corresponding values calculated from the data reduction equations. The applied range of static loading closely approximated the aerodynamic test loads.

	Range of	Measurement
Balance	Static Load	Uncertainty,
Component	Applied, 1b	Absolute, 1b
$^{\mathtt{F}}\mathtt{A}_{\mathtt{T}}$	0.5 - 3	<u>+</u> 0.013
$^{\mathrm{F}}_{\mathrm{N_{F}}}$	0.8 - 12	<u>+</u> 0.008
$\mathbf{F_{N_A}}$	1.2 - 18	<u>+</u> 0.009

Base pressure measurements were made using variable reluctance differential pressure transducers with a range from 0.001 to 0.1 psia. The gages were mounted on the sting with the gage orifice positioned approximately 1/16 in. downstream of the model base.

Two gages were mounted in the nose of the orbiter model ("T" anrangement on a single orifice) to measure p. The gages used were 15-psid strain-gage pressure transducers calibrated at the specific pressure level occurring during each test condition.

The arc chamber pressure, test section pitot pressure, and test section heat-transfer rates on a hemisphere-cylinder probe were monitored to determine tunnel flow conditions. The arc chamber reservoir pressure was measured using two strain-gage transducers, each having full-scale calibrated ranges of 5, 10, and 25 thousand psia. The test section pitot pressures were measured using 2.0-psid strain-gage transducers calibrated for the range of the specific test condition. The stagnation heat-transfer rates used in determining the tunnel flow conditions were inferred from measurements made on the cylindrical section of a 1.0 in.-diam hemisphere-cylinder probe using resistance thermometer slug calorimeters. Slug calorimeters have a thin-film platinum resistance thermometer to sense the temperature of an aluminum disk which is exposed to the heat flux to be measured. The calorimeters are optimized to measure a given range of heat transfer by appropriate selection of the aluminum disk thickness.

Detailed information about the force, heat-transfer, and pressure instrumentation may be found in Refs. 2, 3, and 4.

TEST FACILITY DESCRIPTION

The von Karman Gas Dynamics Facility (VKF) Hypervelocity Wind Tunnel (F) is an arc-driven wind tunnel of the hotshot type (Refs. 3 and 4) and is capable of providing Mach numbers from about 7.5 to 20 over a Reynolds number per foot range from 0.05×10^6 to 70×10^6 . Tests are conducted in the 108-in.-diam test section (M $_{\!\scriptscriptstyle \infty}$ = 14 to 20) using a 4-deg half-angle conical nozzle. The range of Mach numbers is obtained by using various throat diameters. Tests are conducted in the 54-in.-diam test section ($M_m = 8$ to 16) utilizing contoured nozzles as shown in Fig. 2. The M_{∞} = 8, 12, and 16 contoured nozzles have 25-, 40-, and 48in. exit diameters, respectively, which connect to the 54-in.-diam test station and provide a free-jet exhaust. The gas for aerodynamic and aerothermodynamic testing is nitrogen. Air is used for combustion tests. The test gas is confined in either a $1.0-\text{ft}^3$, a $2.5-\text{ft}^3$, or a $4.0-\text{ft}^3$ arc chamber, where it is heated and compressed by an electric arc discharge. The increase in pressure results in a diaphragm rupture with the subsequent flow expansion through the nozzle. Test durations are typically from 50 to 200 msec. Shadowgraph and schlieren coverage are available at both test sections.

This test was conducted in the 108-in.-diam test section of the conical nozzle at M_{∞} = 19 with nitrogen as the gas. The 1.0-ft³ volume are chamber was used, and useful test times up to approximately 50 msec were obtained. Because of the relatively short test times, the model wall temperature remained essentially invariant from the initial value

of approximately $540^{\circ}R$; thus T_w/T_o^{\simeq} 0.12 and approximates the condition of practical interest for reentry vehicles.

TEST PROCEDURE

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The test objective was to determine the static stability and axial— ψ force characteristics of the modified Vehicle 4 Orbiter configuration at Mach number 19 over a Reynolds number (Re_{∞} , ℓ) range from 0.1 x 10^6 to 0.4 x 10^6 at an angle of attack of 30 deg. The elevon and body flap deflection angles were varied for determination of control effectiveness. The primary model configuration tested had all the control surfaces at zero deflection angle, including the speed brake, which was fixed at zero deflection throughout the test series.

A series of runs was made with both the elevons and body flap positioned at their positive deflection limits (δ_e = 15 deg, δ_{BF} = 16.3 deg). This series was tested primarily to verify the trim capability of the configuration at these control surface settings. Both these series of runs were made at the two Reynolds number conditions.

Additional runs were made during both test series with the model inverted (ϕ = 180 deg) and the model nose pitched toward the bottom of the tunnel. These runs were made to assist in determining the corrections to apply to the data for small tunnel flow nonuniformities. One run was made with both the elevons and the body flap positioned at their negative deflection limits ($\delta_{\rm e}$ = -40 deg, $\delta_{\rm BF}$ = -11.7 deg). A complete test summary indicating the primary variables during the test is given in Table II.

The method of determining the tunnel flow conditions is briefly summarized as follows: instantaneous values of reservoir pressure (p_0)

are measured and an instantaneous value of the stagnation heat transfer rate (\dot{q}_{∞}) is inferred from a direct measurement of a shoulder heat rate on a 1.0 in.-diam hemisphere cylinder heat probe. Total enthalpy (H_{0}) is calculated from p'_{0} , \dot{q}_{0} , and the heat probe radius, using Fay-Riddell theory, Ref. 5. The value of H_{0} determined in this manner and the image was a reservoir-pressure are then used to determine corresponding values of reservoir temperature, density, and entropy from tabulated thermodynamic data for nitrogen (Ref. 6). The reservoir conditions, the measured value of p'_{0} , and the assumption of isentropic flow in the nozzle are then used to compute the free stream conditions. The basic procedure followed in this computation is given in Refs. 7 and 8.

A summary of the reservoir and free-stream conditions is given in Table I.

All data were recorded on a 70-channel digitial system capable of scanning all channels in 1 msec and storing up to 150 scans of data.

Basic data reduction was done off-line on a digital computer. As a backup to the digital system, as well as to provide a quick look at the data results, the output of each data channel was also recorded on an oscillograph.

DATA REDUCTION

The model nose p_0^* measurements were used in the calculations for determining the free-stream test section conditions. The force data are normalized by the dynamic pressure, which is thus dependent on the measured model nose pressure.

Since the Tunnel F nozzle providing flow in the 108-in.-diameter test section is conical, source flow effects are present. Adjustments were made to the data to correct for these following the discussion of source flow corrections in Ref. 11. Corrections were determined assuming the pressure coefficient at any station on the "flat-bottomed" orbiter vehicle could be described by the Newtonian expression as a function of angle of attack and source flow angle. The calculated corrections indicated a 0.22-percent rearward shift in $X_{\rm cpN}/2$ was required to correct for source flow. The normal— and axial-force coefficient corrections were less than 1 percent and were considered insignificant when compared to the measurement uncertainties; thus no corrections to $C_{\rm N}$ and $C_{\rm A}$ were made.

Additional corrections to $X_{\rm cpN}/\ell$ and $C_{\rm N}$ were applied to compensate for flow nonuniformities and a source flow angle resulting from the location of the model in the test section. These corrections were determined from a comparison of the aerodynamic data obtained with the model in the normal upright mode and data obtained with the model and balance inverted (ϕ = 180 deg) and pitched toward the bottom of the tunnel. The model was tested in the top half of the tunnel with the

trailing edge of the body flap approximately 1 in. above the tunnel centerline for the inverted position. The accompanying source flow angle and the flow nonuniformities were accounted for by averaging the $X_{\rm CPN}/\ell$ and $C_{\rm N}$ coefficients for the upright and inverted runs for each of the respective configurations at each of the Reynolds number conditions. The resulting corrections were a maximum 2-percent change in $C_{\rm N}$ and a maximum 0.4-percent shift in $X_{\rm CPN}/\ell$. The pitching moments were recomputed to reflect the corrections to the center of pressure, $X_{\rm CPN}/\ell$, and the normal-force coefficient, $C_{\rm N}$.

The following constants were used to reduce the data:

Parameter		Full Sca	<u>le</u>	Model S	<u>Scale</u>
Reference Area (S _{ref})		2690.0 f	t ²	38.736	in. ²
Reference Chord (1 _{ref})		474.8 i	n.	4.748	in.
Reference Span (b _{ref}) (wing span)		936.7 i	n.	9.367	in.
Moment Reference Center	XMRP	1076.68	in. X _o	10.768	in. X _o
	YMRP	0.0	in. Y _o	0.0	in. Yo
	ZMRP	375.0	in. Z _o	3.750	in. Z _o
Body Reference Length (l)	1290.3	in.	12.903	ın.
Base Area (A _b)		421.7	in^2	6.072	in. ²

The NASA/LaRC viscous interaction parameter is defined as:

$$\overline{V}_{\infty}^{\dagger} = \frac{M_{\infty} \sqrt{C_{\infty}^{\dagger}}}{\sqrt{Re_{\infty}} \ell}$$

where

$$C_{\infty}^{\dagger} = \begin{bmatrix} \frac{T^{\dagger}}{T_{\infty}} \end{bmatrix}^{K} \begin{bmatrix} \frac{T_{\infty} + 122.1 \times 10^{-(5/T_{\infty})}}{T^{\dagger} + 122.1 \times 10^{-(5/T_{\infty})}} \end{bmatrix}^{J}$$

with the Monaghan's empirical relationship (reference 12 given by:*

$$\frac{T'}{T_{\infty}} = 0.468 + 0.532(\frac{T_{W}}{T_{\infty}}) + 0.195(\frac{\gamma - 1}{2}) M_{\infty}^{2}$$

where

 T_{∞} = Freestream static temperature, degrees Kelvin

 T_w = Wall temperature (367°K), degrees Kelvin

T' = Reference temperature, degrees Kelvin



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and

K and J are empirical constants. For nitrogen, K = 0.5 and J = 1.0

The hypersonic viscous parameter is also given in the tabulated data and was calculated by:

$$\overline{V}_{\infty} = M_{\infty} \sqrt{C_{\infty}} / \sqrt{R_{e_{\infty}} \ell}$$

where

 $\sqrt{C_{\infty}} = \mu_W^T_{\infty} / \mu_{\infty}^T_W$ (Chapman-Rubesin viscosity coefficient)

^{*} These equations are based on temperature in ${}^{\rm o}{\rm K}$ but the tab. data are ${}^{\rm o}{\rm R}$ units.

DISCUSSION OF RESULTS

The uncertainties in the monitor probe measurements (p_o^i and \dot{q}_o) and arc chamber measurements (p_o^i) considering both static load calibrations, system errors, and data repeatability, are estimated to be \pm 4, \pm 7, and \pm 5 percent, respectively. The p_o^i and p_o uncertainties are based on the average of two measurements and the uncertainty of \dot{q}_o on the inferred value from the average of two probe shoulder measurements. These values were used to estimate uncertainties in the tunnel flow parameters using the Taylor series method of error propagation. Representative parameters are given below.

Uncertainty (+), percent

M_{∞}	Re_{∞} l	T_{∞}	$\underline{p_{\infty}}$	\underline{q}_{∞}	<u>q</u> o	p _o	$\frac{\mathbf{p_{0}^{t}}}{\mathbf{p_{0}^{t}}}$
1.5	12	7	6	4	7	5	4

The uncertainties in the calculated force data were estimated by using the Taylor series method of error propagation to combine the uncertainties in each measurement occurring in the calculations. In general, it is estimated that for nominal loads the uncertainty in the force measurements is \pm 6 percent for each balance component. This uncertainty includes calibration linearity and repeatability, instrumentation system error, and errors introduced by dynamic effects resulting from the impulsive operating nature of the facility. The uncertainty of \pm 6 percent of each balance component measurement combined with a \pm 4

percent uncertainty in the dynamic pressure gives an uncertainty, in the force coefficient C_N , of \pm 6 percent for the load distribution observed during this test. An uncertainty of \pm 6 percent of the measured axial force combined with a \pm 4 percent uncertainty in the dynamic pressure gives an uncertainty in C_A of \pm 7 percent.

The absolute uncertainities in pitching-moment and center of pressure location were determined using the Taylor series method of error propagation. The uncertainties are primarily a function of the load distribution of the normal-force component measurements with the axial force component being a minor influence.

Absolute Uncertainties

C _m	$x_{cp_N/\ell}$
+0.0163	+0.0076

The above-quoted percent uncertainties in C_N and C_A and the absolute uncertainties in C_m and $X_{\text{cp}_N/\ell}$ apply to all the tabulated data presented in this report. It should be noted that these uncertainties apply to each data point and are not necessarily indicative of the overall uncertainty of a force coefficient when the data are plotted versus some parameter, e.g., \overline{V}_o^1 , and a fairing is made through all the data. The following near-minimum load uncertainties were determined using the balance residuals as discussed under Instrumentation in conjunction with the Taylor series method of error propagation and are included here to indicate the lower resolution limits of the balance.

Near-Minimum Load Uncertainties

Nominal Re∞ℓ	Nominal q_{∞}	C <u>_</u>	C _N	C _m
0.35	0.50	0.00067	0.00062	0.00020
0.12	0.17	0.00197	0.00183	0.00059

However, for this report the uncertainty levels to be applied to the data are not the above near-minimum load uncertainties but rather the previously mentioned percent C_N and C_A uncertainties of \pm 6 and \pm 7 percent, respectively, and the absolute uncertainty of \pm 0.0163 for C_m and \pm 0.0076 for $X_{\text{CPN/2}}$. The model attitude was set prior to each run; the pitch angle is estimated to be accurate within \pm 0.10 deg. The estimated uncertainties for the model base pressure measurements are \pm 10 percent.

All of the data taken during this test series were at an approximate Mach number of 19 and at an angle of attack of 30 deg. Analysis of these data over the Reynolds number range tested and comparisons with previous AEDC data obtained at Mach numbers of 8, 10, and 16 show a definite dependence of the aerodynamic characteristics of the Orbiter configuration upon the visous parameter $\overline{V}_{\infty}^{\dagger}$ (hence altitude and velocity). A detailed discussion of the $\overline{V}_{\infty}^{\dagger}$ parameter can be found in Ref. 9.

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- 11. Allen, E. C., "Pretest Report for an Investigation in the AEDC-VKF Tunnel "F" to Verify the Hypersonic Stability and Control Characteristics of the 0.010-Scale Model (51-0) of a Modified Vehicle and Orbiter (Test 0A160)," Rockwell Report SD75-SH-0044, February 15, 1975.
- Bertram, Mitchel H., "Hypersonic Laminar Viscous Interaction Effects on the Aerodynamics of Two-Dimensional Wedge and Triangular Planform Wings," NASA-TN-D-3523, August 1966.

24

Table I. Test Conditions

Run No.*	Time,	P _O , psia	To,	qo Btu/ft ² sec	p'o psia	$p_{\infty} \times 10^3$, psia	$\rho_{\infty} \times 10^{6}$, slugs/ft ³	q_{∞} , psia	υ _ω , ft/sec	M _∞	Re _{∞ &} x 10	\overline{V}_{∞}
4998	94	4843	5171	42.1	0.32	0.588	0.668	0.17	8619	20.5	0.11	0.057
4999	90	4631	5123	40.5	0.31	0.559	0.643	0.16	8573	20.5	0.11	0.058
5000	70	8839	4977	78.6	1.21	2.92	2.61	0.65	8466	17.9	0.34	0.029
5001	90	8142	4711	66.5	1.01	2.31	2.31	0.54	8214	18.3	0.32	0.030
5002	90	8210	4782	70.0	1.08	2.52	2.42	0.58	8281	18.1	0.33	0.029
5003	110	3950	5513	41.1	0.26	0.481	0.503	0.14	8914	20.3	0.08	0.067
5004	100	6999	3969	48.7	0.87	1.92	2.41	0.49	7477	18.7	0.38	0.028
5005	60	3749	5142	47.8	0.42	0.966	0.891	0.23	8568	18.3	0.12	0.049
5006	60	3603	5190	45.9	0.38	0.849	0.794	0.20	8612	18.6	0.11	0.052
5008	80	2997	4606	33.4	0.28	0.578	0.666	0.15	8067	19.3	0.11	0.055
5009	80	6944	4572	58.3	0.85	1.91	2.01	0,45	8071	18.4	0.29	0.032
5010	80	3082	4757	37.1	0.32	0.680	0.724	0.17	8209	18.9	0.11	0.054
5011	60	8121	4896	69.5	1.00	2.28	2.19	0.53	8387	18.3	0.30	0.031
5012	90	6439	4519	53.9	0.75	1.67	1.81	0.40	8016	18.6	0.27	0.034

^{*}See Table II for model test attitude and configuration.

7-160 (V41F-28A)		-	DAT	A SE	T/RU		e II MBE		ATION SUMMARY	DATE:	10/10/75	************	
CONFIGURATION	teritories.								/ALUES	NO.	RUN NU	MBERS	
				1	1		Ŷ		MACH	RUNS			
WKBITER (MODEL 51	~	1	0	0	0	0	0	.08	20.3		5003		
		·		0	0	0	0	1.//	20.5		4998		_
			0	0	0	0	0	•12	18.3		5005		_
		+	0	0	0	0	0	.32	18.3		5001		
		1	0	0	0	0	0	.38	18.7		5004		
	30	0	180	0	0	0	0	//	18.6		5006		
-	30	0	180	0	0	0	0	.11	20.5		4999		
	30	ی	180	D	0	0	0	.27	18.6		5012		_
	30	0	180	0	0	0	0	.34	17.9		5000		_
	30	0	0	15	16.3	_0	0	-11	19.3		5608		
	30	0	0	15	16.3	0	0	.29	18.4		1 - 1		-
	30	0	180	15	16.3	0	0	-11					-
	30	0	180	15	16.3	0	o			7			
	30	0				0	0	,					-
							_		100		0002		-
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													-
										- -			-
12 10	e de engige							P-71-2-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-					=
	1.E.					1, 1, 1,			49 DL./.D		 		-
$\beta = IV(2) = x$			-						'S' DATA-RH	O. VBAR U.	IDVAD (1)	DVAD (2)	_
	CONFIGURATION ORBITER (MODEL 5) 13 19 N. ICAB ICAB LES	CONFIGURATION . a CONFIGURATION . a CONFI	CONFIGURATION SCHO. a B CRBITER (MODEL 51-4) 30 0 30 0	CONFIGURATION SCHO. CONFIGURATION SCHO. G	CONFIGURATION SCHO. CONFIGURATION SCHO. CONFIGURATION SCHO. CONFIGURATION SCHO. CONFIGURATION SCHO. CONFIGURATION SCHO. CONFIGURATION SCHO. CONFIGURATION SO O O CONFIGURATION SO SO O CONFIGURATION SO O CONFIGURATION SO O CONFIGURATION SO O CONFIGURATION SO O CONFIGURA	CONFIGURATION CONFIG	CONFIGURATION SCHD. (a) B	CONFIGURATION SCHD. SAR SAR SAR SAR	CONFIGURATION SCHO. SCHOL PARAMETERS/A QRBITER (MODEL 51-4) 30 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	CONFIGURATION SCHOL SCHO	CONFIGURATION CONFIGURATION	CONFIGURATION SCHOL PARAMETERS/VALUES NO. RUN NUMBER NO. RUN NUMBE	CONFIGURATION SCHD. FARAMETERS/VALUES NO RUN NUMBERS

TABLE III MODEL DIMENSIONAL DATA

MODEL COMPONENT : BODY - B		
GENERAL DESCRIPTION : Configuration	140A/B orbiter fu	selage .
NOTE: B26 is identical to B24 except	underside of fuse	lage has been
refaired to accept W116.		
MODEL SCALE: 0.010	MODEL DWG NO.: SS	-A00147, Release 12
DRAWING NUMBER . <u>VL70-000143B</u> , -000 VL70-000140A,00	0200, -000205,0 00140B	060 89, - 000145
DIMENSIONS :	FULL SCALE	MODEL SCALE
Length (OML: Fwd Sta. $X_0=235$) Length (IML: Fwd Sta. $X_0=238$)		12.933 12.903
Max Width (@ X _O = 1528.3), In.	264.0	2.640
Max Depth (@ $X_0 = 1464$), In.	250.0	2.500
Fineness Ratio	0.264	0.264
Area - Ft ²		
Max. Cross-Sectional	340.88	0.034
Planform		
Wetted		
Base		

MODEL COMPONENT : CANOPY - C9		
GENERAL DESCRIPTION : Configuration 3A	. Canopy used	with fuselage B ₂₆ .
MODEL SCALE: 0.010 MODE		A00147, Release 12
DRAWING NUMBER		
· · · · · · · · · · · · · · · · · · ·		
DIMENSIONS :	FULL SCALE	MODEL SCALE
Length ($I_0 = 434.643$ to 578), In.	143.357	1.434
Max Width (@ $X_0 = 513.127$), In.	152.412	1.524
Max Depth (@ $X_0 = 485.0$), In.	25.000	0.250
Fineness Ratio		
Area		
Max. Cross-Sectional		-
Planform	·	
Wetted		**************************************
Base		

MODEL COMPONENT: ELEVON - E26		-
GENERAL DESCRIPTION: Configuration 140A	/B orbiter elevor	S
MODEL SCALE: 0.010 MODEL D	WG: SS-A00148. R	elease 6
DRAWING NUMBER: VL70-000200, -00	6089, -006092	
DIMENSIONS:	FULL-SCALE	MODEL SCALE
Area - Ft ²	205.25	0.0205
Span (equivalent), In.	346.68	3.467
Inb'd equivalent chord, In.	115.3	1,153
Outb'd equivalent chord, In.	_55.189	0.552
Ratio movable surface chord/ total surface chord		
At Inb'd equiv. chord	0.214	0.214
At Outb'd equiv. chord	0.400	0.400
Sweep Back Angles, degrees		
Leading Edge	0.00	0.00
Tailing Edge	- 10.056	-10,056
Hingeline Product of area & c)	0.00	0.00
Area Moment (Normatotochingeobine), F	t ³ 1 <u>518.27</u>	0.0015
Mean Aerodynamic Chord, In.	88.777	0.888

MODEL COMPONENT : BODY FLAP - F7		
GENERAL DESCRIPTION :Configuration	140A/B orbiter b	ody flap
MODEL SCALE: 0.010 MODEL	DWG: SS-A00147.	Release 12
DRAWING NUMBER . VL70-000140A, -00	·	
* [•
* *		
DIMENSIONS .	FULL SCALE	MODEL SCALE
Length $(X_0 = 1520 \text{ to } X_0 = 1613)$), <u>In. 93.00</u> 0*	0.930
Max Width , In.	262.0	2.620
Max Depth (@ $X_0 = 1520$), In.	23.000	0.230
Fineness Ratio		
Area - Ft ²		
Max. Cross-Sectional		
Planform	142.6	0.014
Wetted		
Base	41.847	0.004

^{*}Model dim. measured from Model Sta. 15.20

TABLE III. - Continued.

MODEL COMPONENT : OMS/RCS PODS	<u>- м</u> ,	
GENERAL DESCRIPTION:Configurat	ion 140A/B Orbiter	OMS/RCS pods
MODEL SCALE: 0.010 MC	DEL DRAWING: SS-AC	00147, RELEASE 12
DRAWING NUMBER: VL70-000145		
		·
DIMENSIONS :	FULL SCALE	MODEL SCALE
Length (OMS Fwd Sta $X_0=1233$.0),In. 327.000	3,270
Max Width (@ $X_0 = 1450.0$),	In. 94.50	0.945
Max Depth (@ $X_0 = 1493.0$),	In. <u>109.000</u>	1.090
Fineness Ratio	***************************************	
Area		
Max. Cross—Sectional		
Planform		·
Wetted		
Base		

MODEL COMPONENT: OMS NOZZLES - N28		•
GENERAL DESCRIPTION: Configuration 140A/B or	biter OMS Nozz	les
	·•	
MODEL SCALE: 0.010		
DRAVING NUMBER: VL70-000140A (Location). SS	-A00106, Relea	se 5 (Contour)
DIMENSIONS:	FULL SCALE	MODEL SCALE
MACH NO.	•	
Length - In. Gimbal Point to Exit Plane	,	
Throat to Exit Plane		
i Diameter - In.		
Exit. Throat		
Inlet		
rea - ft ² Exit		
Throat	<u> </u>	
Gimbal Point (Station) - In. Left Koxxex Nozzle		
Left Mark Nozzle	1518.00	15.180
\mathbf{Y}_{O}	- 88.0	- 0.880
^Z 0	492.0	4.920
Right Lover Nozzles	2 5 4 6	35.40
${f x}_{f O} {f y}_{f O}$	1518.0 88.0	15.180 0.880
z_0^0	492.0	4.920
Null Position - Deg.		
Left Weper Nozzle		
Pitch Yaw	<u> 15°49'</u> 12°17'	15°49' 12°17'
1		
Right RESERT Nozzle ' Pitch	15°49'	15°49'
Yaw	12°17'	12°17'

TABLE III (Cont'd)

MODEL COMPONENT: RUDDER - R		······································
GENERAL DESCRIPTION: Configuration 140C orb	iter rudder (iden	ntical to
MODEL SCALE: 0.010		
DRAWING NUMBER: VI.70-000146B0	000095	
DIMENSIONS:	FULL-SCALE	MODEL SCALE
Area - Ft ²	100.15	0.010
Span (equivalent), In.	201.00	2.010
Inb'd equivalent chord, In.	91.585	0.916
Outb'd equivalent chord, In.	50.833	0.508
Ratio movable surface chord/ total surface chord		
At Inb'd equiv. chord	0.400	0.400
At Outb'd equiv. chord	0.400	0.400
Sweep Back Angles, degrees		•
Leading Edge	-	
Tailing Edge	26.25	26.25
Hingeline Product of Area & c) 3	34.83	34.83
Area Moment (Normatico Name ** The), Ft 3	610.92	0.0006
Mean Aerodynamic Chord, In.	73.2	0.732

TABLE III (Cont'd)

MODEL COMPONENT: VERTICAL - V8		
GENERAL DESCRIPTION: Configuration 14	OC orbiter vertical t	ail (identical
to configuration 140A/B vertical tail)		
MODEL SCALE: 0.010		
DRAWING NUMBER: VI70-000140C, -000146B		
dimensions:	FULL SCALE	MODEL SCALE
TOTAL DATA		
Area (Theo) - Ft ² Planform Span (Theo) - In. Aspect Ratio Rate of Taper Taper Ratio Sweep-Back Angles, Degrees. Leading Edge Trailing Edge O.25 Element Line Chords: Root (Theo) WP Tip (Theo) WP MAC Fus. Sta. of .25 MAC W.P. of .25 MAC B.L. of .25 MAC	413.253 315.72 1.675 0.507 0.404 45.000 26.25 41.13 268.50 108.47 199.81 1463.35 635.52 0.00	0.01 3.157 1.675 0.507 0.404 45.000 26.25 41.13 2.685 1.085 1.998 14.633 6.355 0.0
Airfoil Section Leading Wedge Angle - Deg. Trailing Wedge Angle - Deg. Leading Edge Radius	10.00 14.92 2.00	10.0 1R.92 0.020
Void Area	13.17	0.0013
Blanketed Area	0.00	0.00

TABLE III (Cont'd)

MODEL COMPONENT: WING-W116		
REVERA_ DESCRIPTION: Configuration 4		
TEST VO.	DWG. NO.	
DIMENSIONS:	FULL-SCALE	MODEL SCALE
TOTAL DATA		•
Area (neo.) Ft ²	2690.00	0.240
Span (Theo In.	936.68	0.269 9.367
Aspect Ratio	2.265	2.265
Rate of Taper	1.177	1.177
Taper Ratio Dihedral Angle, degrees	0.200 3.500	0.200 3.500
Incidence Angle, degrees	0.500	0.500
Aerodynamic Twist, degrees		
Sweep Back Angles, degrees Leading Edge	45.000	<u>45.000</u>
Trailing Edge	- 10.026	<u> </u>
0.25 Element Line	35.209 .	35.209
Chords:	400 al	4 800
Root (Theo) B.P.O.O. Tip, (Theo) B.P.	689.24 137.85	$\frac{6.892}{1.379}$
MAC	474.81	4.748
Fus. Sta. of .25 MAC	1136.83	11.368
W.P. of .25 MAC B.L. of .25 MAC	290.58 182.13	2.906 1.821
EYPOSED DATA	**************************************	
Area (Theo) Ft	<u> 1751.50</u>	0.175
Span, (Theo) In. BP108	720.68	<u> </u>
Aspect Ratio Taper Ratio	2.059 0.245	2.059 0.245
Chords		
Root BP108	562.09	5.621
Tip 1.00 <u>b</u>	137.85	1.379
MAC	392.83 1185.98	3,928
Fus. Sta. of .25 MAC W.P. of .25 MAC	294.30	<u>11.860</u> <u>2.943</u>
B.L. of .25 MAC	251.77	2.518
Airfoil Section (Rockwell Mod NASA) XXXX-64		
Root b ≠	0.113	0.113
Tip b= 2	0.120	0.120
Data for (1) of (2) Sides		
Leading Edge Cuff Planform Area Ft ²		A 627
Leading Edge Intersects Fus M. L. 0 Sta	113.18 500.00	<u>0.011</u> 5.00
Leading Edge Intersects Ving @ Sta	1024.00	10.240
- · · · · · · · · · · · · · · · · · · ·		· · · · · · · · · · · · · · · · · · ·

Notes:

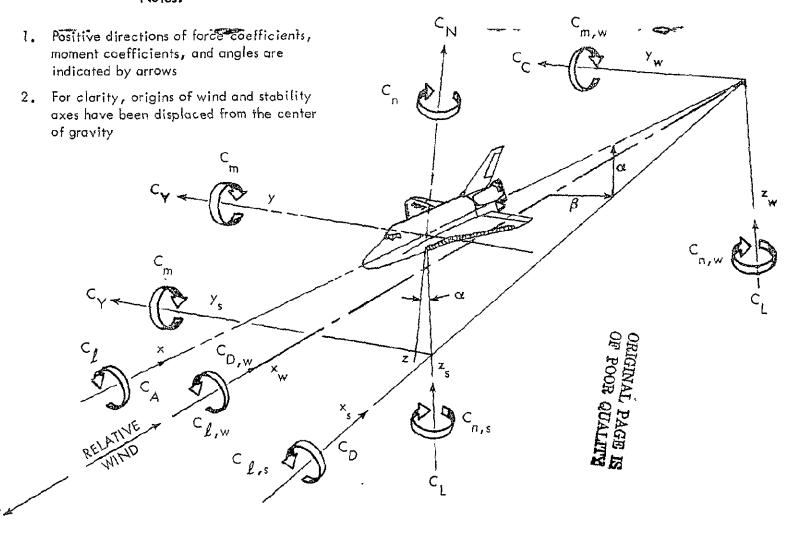


Figure 1. Axis Systems

936.73

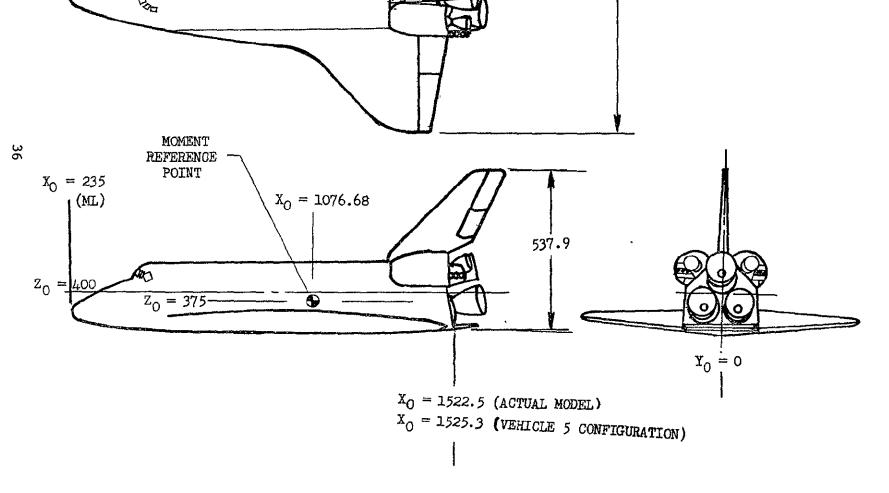


Figure 2. Model Sketch

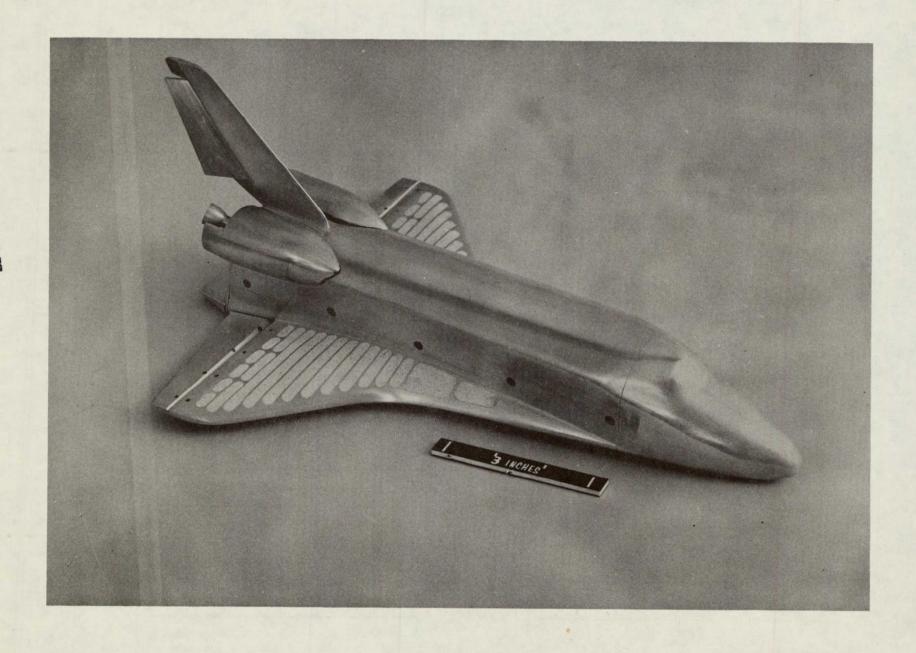


Figure 3. - Model Photograph.

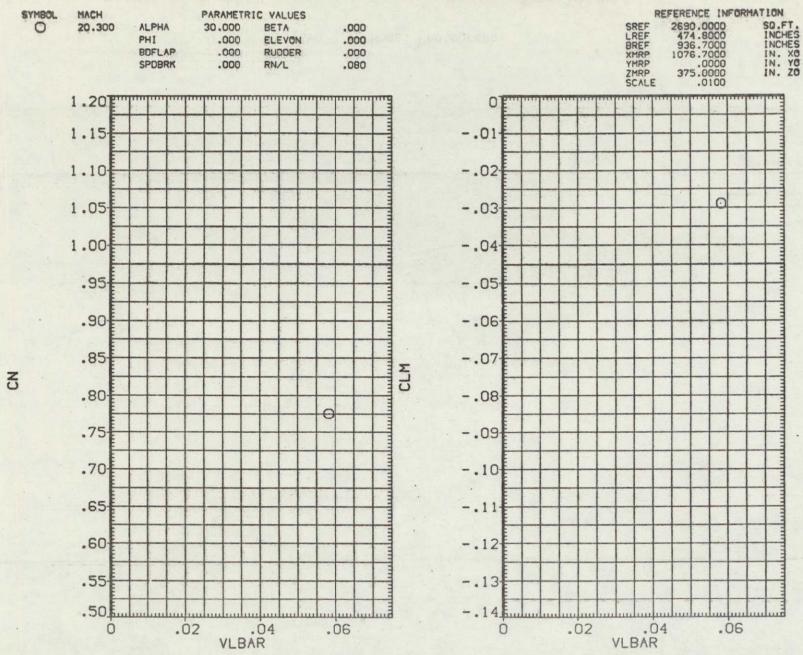


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

DATE D9 DEC 75	OA160 TABULATED SOURCE DATA	•	PAGE	10
DATE US DEC 13	AUTOD INDOPENIED DOGING BUILD			

			OA160.	(V41F-28/	A) (B26C9	F7M7N2B) (WI II	6E26) (V8R5)		(SVAO	14) (09 D	EC 75)
	REFEREN	ICE DATA							PARAMETRI	DATA	
SREF = LREF = BREF = SCALE =		1.FT. XMRP ICHES YMRP ICHES ZMRP	= 1076.700 = .000 = 375.000	0 IN. YO				ALPHA = PH1 = BDFLAP = SPDBRK =	30.000 .000 -11.700 .000	BETA = ELEVON = RUDDER = RN/L =	.000 -40.000 .000 .320
		RUN NO.	5002/ 0						•	-	
MACH 17.800 18.100 17.900	90.000	RHO 2.50000 2.42000 2.29000		U 84.00000 81.00000 99.00000	QDOT 82.40000 70.00000 68.00000	† 94.28000 84.27000 85.68000	P .02910 .02520 .02420	1.08000	8210.00000	T(0) 5162.00000 4782.00000 4790.00000	Q(PSI) .65000 .58000 .54000

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DATE 09 DEC 75

OA160 TABULATED SOURCE DATA

PAGE 9 OA160, (V41F-28A) (B26C9F7M7N28)(W116E26)(V8R5) (SVA011) (09 DEC 75) REFERENCE DATA PARAMETRIC DATA SREF = 2690,0000 SQ.FT. XMRP = 1076.7000 IN, XO ALPHA = 30.000 BETA = 474.8000 INCHES LREF = YMRP = .0000 IN. YO PHI = .000 ELEVON = 15.000 BREF = 935.7000 INCHES ZMRP * 375.0000 IN. ZO BDFLAP = 16.300 RUDDER = .000 SCALE = .0100 .000 SPOBRK = RN/L = .290 RUN NO. 5009/ 0 MACH TIME RHO VBAR QDOT PITOT P(0) T(0) Q(PSI) 18.200 70.000 2.14000 .02220 .03140 8317 00000 66.80000 84.26000 .96000 7565.00000 4828.00000 .51000 18.400 80 000 2.01000 .03190 8071.00000 58.30000 77.22000 .01910 .85000 6944.00000 4572.00000 .45000 18,600 90.000 1.84000 .03300 7929,00000 52.40000 73.19000 .01660 .75000 6338.00000 4430.00000 .40000 0A160, (V41F-28A) (826C9F7M7N28)(W116E26)(V8R5) (SVA012) (09 DEC 75) REFERENCE DATA PARAMETRIC DATA SREF = 2690.0000 SQ.FT. XMRP = 1076.7000 IN. XO ALPHA = .000 30.000 BETA = LREF = 474.8000 INCHES YMRP = 0000 IN. YO PHI = 180 000 ELEVON = 15.000 BREF = 936 7000 INCHES ZMRP = 375.0000 IN. ZO BDFLAP = 16.300 RUDDER = .000 SCALE = .0100 SPDBRK = RN/L ≖ .000 . 130 RUN NO. 5010/ 0 MACH TIME RHO **VBAR** QDOT PITOT P(0) Q(PSI) 18.700 60.000 .98100 .04540 7998.00000 39.40000 73.44000 .00889 .41000 3689.00000 4530.00000 .22000 18.700 70.000 .88300 .04790 7995.00000 37.30000 73.31000 .00798 .36000 3333.00000 4530.00000 .20000 18.900 80.000 .72400 .05360 8209.00000 37.10000 76.17000 .00680 .32000 3082.00000 4757.00000 .17000 19 500 90.000 .67900 .05370 7743 00000 29.20000 63.43000 .00531 .26000 2849.00000 4274.00000 .14000 OA16G. (V41F-28A) (B26C9F7M7N28)(W116E26)(V8R5) (SVA013) (09 DEC 75) REFERENCE DATA PARAMETRIC DATA SREF = 2690.0000 SQ.FT. XMRP = 1076.7000 IN. XO ALPHA = 30.000 BETA = .000 474.8000 INCHES YMRP = .0000 IN. YO PHI = 180,000 ELEVON = 15.000 BREF = 936.7000 INCHES ZMRP = 375.0000 IN. 20 BDFLAP = 16.300 RUDDER = .000 SCALE = .0100 SPDBRK = .000 RN/L = .330 RUN NO. 5011/ 0 MACH TIME RHO **VBAR** U QDOT PITOT Q(PSI) P(0) T(0) .03120 8387.00000 18.300 60.000 2.19000 69.50000 84.68000 .02280 1.00000 8121.00000 4896.00000 .53000 18.500 65.000 2.45000 .02840 7788.00000 56.80000 71.14000 .02150 .96000 7713.00000 4272.00000 .52000

OA160 TABULATED SOURCE DATA

PAGE 8

		0A160, (V41F-8	28A) (B26C9	9F7M7N28) (W11	6E26) (V8R5)		(SVAC	(80 (80	DEC 75)
	REFERENCE DATA						PARAMETRI		
SREF * LREF = BREF * SCALE *	2690.0000 SQ.FT. XMRP 474.8000 INCHES YMRP 936.7000 INCHES ZMRP	= .0000 IN. YO)))			ALPHA = PHI = BDFLAP = SPOBRK =	30.000 180.000	BETA = ELEVON = RUDDER = RN/L *	.000 .000 .000 .280
	RUN NO	. 5012/ 0							
MACH 18.200 18.200 18.300 18.600	TIME RHO 60.000 2.02000 70.000 2.00000 80.000 1.83000 90.000 1.81000	VBAR U.03320 8786.00000 03290 8571.00000 .03420 8466.00000 .03350 8016.00000	QDOT 78.60000 71.80000 65.70000 53.90000	T 93.26000 89.51000 86.29000 74.73000	P .02320 .02210 .01950 .01670	.95000 .85000	7770.00000 7073.00000	T(O) 5332 00000 5102.00000 4993.00000 4519.00000	Q(PSI) .54000 .51000 .46000 .40000
		0A160, (V41F-2	8A) (826C9	F7M7N28) (WI 16	6E26) (V8R5)		(SVAO	09) (09)	DEC 75)
	REFERENCE DATA					(7)	PARAMETRI		
SREF = LREF = BREF = SCALE =	2690.0000 SQ.FT. XMRP 474.8000 INCHES YMRP 936.7000 INCHES ZMRP .0100	■ 1075.7000 IN. XO ■ .0000 IN. YO ■ 375.0000 IN. ZO				ALPHA = PHI = BOFLAP = SPDBRK =	30.000 180.000 .000	BETA ** ELEVON ** RUDDER ** RN/L **	.000 .000 .000 .350
	RUN NO.	5000/ 0							
MACH 17,900 18.000 18.100 18 300	TIME RHO 70.000 2.61000 80.000 2.58000 90 000 2.44000 100.000 2.36000	VBAR U .02870 8466.00000 .02830 8138.00000 02880 7960.00000 .02880 7703.00000	QDOT 78.60000 68.00000 61.20000 53.60000	T 90.52000 82.05000 77.49000 71.55000	P .02920 .02610 .02330 .02080	1.11000	P(Q) 8839.00000 8112.00000 7440.00000 6769.00000	4631.00000 4453.00000	Q(PSI) .65000 .59000 .54000
		0A160, (V41F-28	BA) (B2609F	7M7N28)(W116	E26) (V8R5)		(SVA01	10) (09 5	EC 75)
	REFERENCE DATA						PARAMETR (
SREF = LREF = BREF = SCALE =	2690.0000 SQ.FT. XMRP 474 9000 INCHES YMRP 936.7000 INCHES ZMRP .0100	= 1076.7000 IN. X0 = .0000 IN. Y0 = 375.0000 IN. Z0				ALPHA = PHI = BDFLAP = SPDBRK =	30.000 .000 16.300 .000	BETA = ELEVON = RUDDER = RN/L =	.000 15.000 .000 .100
	RUN NO.	5008/ 0							
MACH 18.900 19.300	TIME RHO 70.000 .67400 80.000 .66600	VBAR U .05670 8556.00000 .05540 8067.00000	QDOT 41.30000 53.40000	T 82.83000 70.38000	P .00689 .00578	PITOT .32000 .28000	P(0) 3251,00000 2997,00000	T(0) 5129.00000 4606.00000	Q(PSI) .17000 .15000

DATE 09 DEC 75

OA160 TABULATED SOURCE DATA

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OA160, (V41F-28A) (B26C9F7M7N2B)(W116E26)(V8R5) (SVA005) (09 DEC 75) REFERENCE DATA PARAMETRIC DATA SREF 2690.0000 SQ.FT. 474.8000 INCHES XMRP 1076,7000 IN. XO ALPHA = 30,000 BETA .000 LREF YMRP .0000 IN. YO PHI = .000 ELEVON = .000 BREF = 936.7000 INCHES ZMRP .000 72 375.0000 IN. ZO BDFLAP = RUDDER = .000 SCALE = .0100 SPDBRK = .000 RN/L = .430 RUN NO. 5004/ 0 MACH TIME RHO **VBAR** Ü · QDQT PITOT P(0) Q(PSI) T(0) 18.700 70.000 2.99000 .02540 7631.00000 58.40000 66.90000 .02470 1.13000 9142.00000 4097.00000 .60000 18.600 80,000 2.78000 .02640 7635.00000 56 30000 67.87000 02320 1 05000 8299.00000 4111 00000 .55000 90.000 18.600 2.70000 .02640 7466.00000 51.40000 64 60000 .02150 .97000 7700.00000 3951.00000 .52000 18.700 2.41000 .02800 7477.00000 48.70000 64.56000 .01920 .87000 6999.00000 3969.00000 .49000 0A160, (V41F-28A) (B26C9F7M7N28)(W116E26)(V8R5) (SVA006) (09 DEC 75) REFERENCE DATA PARAMETRIC DATA 2690,0000 SQ.FT. XMRP 1076 7000 IN. XO = ALPHA = ,000 30.000 BETA = LREF 474.8000 INCHES YMRP 223 .0000 IN. YO PHI -180.000 ELEVON # .000 BREF = 936.7000 INCHES ZMRP = 375,0000 IN. ZO BDFLAP = .000 RUDDER * .000 .0100 SPDBRK = .000 RN/L = .100 RUN NO. 5006/ 0 MACH TIME RHO QDOT Q(PSI) PITOT P(0) 18.600 60.000 .79400 .05240 8612.00000 45.90000 86.67000 .00849 .38000 3003.00000 5190.00000 .20000 18.900 70.000 .69500 .05530 8407.00000 39.50000 79.24000 .00679 .32000 3244.00000 4966.00000 .17000 19.300 80.000 .62800 .05740 8171.00000 34.00000 72.00000 .00558 .27000 2962.00000 4715.00000 .15000 0A160, (V41F-28A) (B26C9F7M7N28)(W116E26)(V8R5) (SVA007) (09 DEC 75) REFERENCE DATA PARAMETRIC DATA SREF 2690.0000 SQ.FT. XMRP 1076.7000 IN. XO -ALPHA * 30.000 BETA .000 LREF 474.8000 INCHES YMRP = .0000 IN. YO PHI. 180,000 ELEVON = .000 BREF = 936.7000 INCHES ZMRP = 375.0000 IN. ZO BOFLAP = RUDDER = .000 .000 SCALE = .0100 SPOBRK * RN/L .000 .110 RUN NO. 4999/ 0 MACH TIME **VBAR** RHO **QDOT** PITOT P(0) T(0) Q(PSI) 20.300 70.000 49.20000 40.50000 .68300 .05770 8981.00000 78,50000 .00662 .36000 5454.00000 5573.00000 .19000 27.500 90.000 .64300 .05810 8573.00000 .06040 8422.00000 70,42000 .00559 .31000 4631.00000 5123.00000 .16000 20.700 110.000 .58400 36.30000 66.53000 .00479 ,27000 4204,00000 4961,00000 .14000 DATE 09 DEC 75 CA160 TABULATED SOURCE DATA PAGE 6

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			OA160.	(V41F-28A) (826C9F	7M7N28) (W11	6E26) (V8R5)		(SVAQ	02) (0 9 DE(C 75)
	REFERENCE	DATA							PARAMETRI	DATA	
SREF = LREF = BREF = SCALE =	2690.0000 SQ.F 474.8000 INCH 936.7000 INCH .0100	ÆS YMRP		IN. XO IN. YO IN. ZO				ALPHA = PHI = BOFLAP = SPOBRK =	30.000 .000 .000	BETA = ELEVON = RUDDER = RN/L =	.000 .000 .000 .120
		RUN NO.	4998/ 0								
MACH 20.000 20.500 20.800	TIME 84.000 94.000 104.000	RHO .80200 .66800 .65100	VBAR .05200 8565 .05720 8619 .05670 8271	.00000	QDOT 45.20000 42.10000 36.00000	T 73.39000 71.41000 63.32000	P .00726 .00588 .00508	.32000	4843.00000	T(0) 5110.00000 5171.00000 4795.00000	Q(PSI) .20000 .17000 .15000
			OA160,	(V41F-28A	(B26C9F	7M7N28) (H11	6E26) (V8R5)		(SVAO	03) (09 DE(C 75)
	REFERÊNCE	DATA							PARAMETRI	C DATA	
SREF = LREF = BREF = SCALE =	2690.0000 SQ.F 474.8000 INCF 936.7000 INCF	HES YMRP	= 1076.7000 = .0000 = 375.0000	IN. YO				ALPHA = PHI = BDFLAP = SPOBRK =	30.000 .000 .000	8ETA = ELEVON = RUDDER = RN/L =	.000 .000 .000 .130
		RUN NO.	5005/ 0								
MACH 18.300 18.800 19.000	TIME 60.000 70.000 80.000	RHO .89100 .88300 85400	VBAR .04930 8568 .04780 7968 .04770 7688	3.00000	QDOT 47.80000 36.90000 32.00000	T 87.86000 72.08000 65 54000	P .00966 .00785 .00691	. 36000	3383.00000	T(0) 5142.00000 4501.00000 4216.00000	Q(PSI) .23000 .19000 .17000
			OA160,	(V41F-28A	(B26C9F	7M7N28) (W11	6E26) (VBR5)		(SVAD	04) (09 DE	C 75)
	REFERENCE	E DATA							PARAMETRI	C DATA	
SREF = LREF = BREF = SCALE =	2690.0000 50.1 474.8000 INC 936.7000 INC	HES YMRP		IN. XO IN. YO IN. ZO				ALPHA = PHI = BOFLAP = SPDBRK =	000.08 000. 000. 000.	BETA = ELEVON = RUDDER = RN/L =	.000 .000 .000 .300
		RUN NO.	5001/ 0								
MACH 008.81 18.300	TIME 90.000 100.000	RHO 2.31000 2.02000	VBAR .03000 821 .03230 834		QDOT 66.50000 65.60000	T 80.80000 83.74000	P .02310 .02090	1.01007 0.0010.1 0.00100	P(0) 8142:00000 7437:00000	T(0) 94711.00000 94855.00000	Q(PSI) .54000 .49000

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ST 5					
DATE_09 DEC 75	OA16	50 TABULATED SOURCE DA	STA .	PA	GE 5
_	OA160, (V41F-28A)	(B26C9F7M7N2B) (W116E	(26) (V8R5)	(RVA013) (25 0	CT 75)
REFERENCE DATA				PARAMETRIC DATA	
SREF = 2690.0000 SQ.FT. XMRP LREF = 474.8000 INCHES YMRP BREF = 936.7000 INCHES ZMRP SCALE = .0100	= 1076.7000 IN. XO = .0000 IN. YO = 375.0000 IN. ZO		ALPHA = PHI = BDFLAP = SPDBRK =	30.000 BETA = 180.000 ELEVON = 16.300 RUDDER = .000	.000 15.000 .000
RUN NO.	5011/ 0				
MACH TIME RN/L 18.300 50.000 .30000 18.500 55.000 .37000	CN CAB .8950000088 .8950000086	CAF CLM .1360012000 .1350012000	XCP/L CL .69900 .70700 .70000 .70800	CD L/D .56500 1.25000 .56400 1.25000	VLBAR .02750 .02550
	OA160. (V41F-28A)	(B26C9F7M7N28) (W116E	(26) (V8R5)	(RVA014) (25 0	CT 75)
REFERENCE DATA				PARAMETRIC DATA	
SREF = 2690.0000 SQ.FT. XMRP LREF = 474.8000 INCHES YMRP BREF = 936.7000 INCHES ZMRP SCALE = .0100	= 1076.7000 IN. XO = .0000 IN. YO = 375.0000 IN. ZO		ALPHA = PHI = BOFLAP = SPDBRK =	30 000 BETA = .000 ELEVON = -11.700 RUDDER = .000	.000 -40.000 .000
RUN NO.	5002/ 0				
MACH TIME RN/L 17.800 80.000 .32000 18.100 90.000 .33000 17.900 100 000 .31000	CN CAB .72500 - 00088 .7220000086 .7170000086	CAF CLM .11200 .02440 .11100 .02490 .11000 .02460	XCP/L CL .63800 .57200 .63700 .57000 .63700 .56600	CD L/D .45900 1.24000 .45700 1.25000 .45400 1.25000	VLBAR .02580 .02600 .02670
	OA160, (V41F-28A)	(826C9F7M7N28)(W116E	E26) (V8R5)	(SVA001) (09 D	EC 75)
REFERENCE DATA				PARAMETRIC DATA	
SREF = 2690.0000 SQ.FT. XMRP LREF = 474.8000 INCHES YMRP BREF = 936.7000 INCHES ZMRP SCALE = .0100	= 1076.7000 IN. XO = .0000 IN. YO = 375.0000 IN. ZO	_	ALPHA = PHI = BDFLAP = SPOBRK =	30.000 BETA = .000 ELEVON = .000 RUDDER = .000 RN/L =	.000 .000 .000 .080
RUN NO.	5003/ 0	-	•		
MACH TIME RHO 20.300 110.000 .50300	VBAR U .06700 8914.00000 4	QDOT T 1.10000 77.49000	P PITOT .26000	P(0) T(0) 3950.00000 5513.00000	Q(PSI) .14000

		0A160, (V	1F-28A) (8260	9F7M7N28) (WI I	6E26) (VBR5)		(RVA01	0) (25 00	CT 75)
RE	FERENCE DATA						PARAMETRIC	DATA	
LREF = 474.80	00 SQ.FT. XMRP 00 INCHES YMRP 00 INCHES ZMRP 00	= 1076.7000 IN = .0000 IN = 375.0000 IN	. YO			ALPHA = PHI = BDFLAP = SPOBRK =	30.000 .000 16.300 .000	BETA = ELEVON = RUDDER =	.000 15.000 .000
	RUN NO.	5008/ 0							
MACH TIM 18.900 70. 19.300 80.	000 .10000	CN CAE .8890000 .8950000	095 .17500		XCP/L .70100 .69800	CL .68200 .68900	CD .59600 .59700	L/D 1.14000 1.15000	VLBAR .04970 .04930
		0A160, (V4	1F-28A) (826C	9F7M7N28) (W11	6E26) (V8R5)		(RVA01	1) (25 00	CT 75)
RE	FERENCE DATA			,	ı		PARAMETRIC	DATA	
LREF = 474.80	00 SQ.FT. XMRP 00 INCHES YMRP 00 INCHES ZMRP 00	= 1076.7000 IN = .0000 IN = 375.0000 IN	. YO			ALPHA = PH! = BDFLAP = SPOBRK =	30.000 .000 16.300 .000	BETA = ELEVON = RUDDER =	.000 15.000 .000
	RUN NO.	5009/ 0							
MACH TIM 18.200 70 18.400 80 18.600 90.	00008. 000	CN CAB .8890000 .9000000	081 .14200 079 .14400	-,12300	XCP/L .69900 .70000 .70000	CL .69900 .70800 .70300	CD .56700 .57500 .57400	L/D 1.23000 1.23000 1.22000	VLBAR .02770 .02840 .02950
		0A160. (V4	1F-28A) (B26C	9F7M7N28) (W11	6E26) (V8R5)		(RVA01	2) (25 00	CT 75)
RE	FERENCE DATA						PARAMETRIC	DATA	
LREF - 474.80	00 SQ.FT. XMRP 00 INCHES YMRP 00 INCHES ZMRP 00	= 1076.7000 IN = .0000 IN = 375.0000 IN	. YO			ALPHA * PHI * BDFLAP * SPDBRK *	30.000 180.000 16.300 .000	BETA = ELEVON = RUDDER =	.000 15.000 000
	RUN NO.	5010/ 0							
18.900 80.	000 .15000 000 .13000	CN CAE .8620000 .8830000 .9030000 .9200000	125 .16000 124 .16500 150 .17000	11800 12200	XCP/L .69800 .69900 .70000	CL .66700 .68200 .69700 .70900	CD .56900 .59500 .59900 .61200	L/D 1.17000 1.17000 1.16000 1.16000	VLBAR .04050 .04270 .04750 .04830

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•			0A160	(V41F-28A)	(B26C9F	7M7N28) (W116	6E26) (V8R5)		_ (RVA00	7) נ 25 OCT	75)
	REFERENCE	E DATA							PARAMETRIC	DATA	
SREF = UREF = SCALE =	2690.0000 SQ.F 474.8000 INCH 936.7000 INCH .0100	HES YMRP	= .00	000 IN. XO 000 IN. YO 000 IN. ZO		,		ALPHA = PHI = BDFLAP = SPDBRK =	30,000 180,000 .000 000	BETA = ELEVON = RUDDER =	.000 .000 .000
		RUN NO.	4999/ 0								
MACH 20.300 20.500 20.700	TIME 70.000 90 000 110 000	RN/L .11000 .11000 .10000	CN .78400 .79800 .80000	CAB 00096 00092 00090	CAF .15900 .16400 .16400	CLM 03060 02930 03030	XCP/L .66400 .66300 .66400	CL .59900 .60900 .61100	CD .53000 .54100 .54200	L/D 1.13000 1.13000 1.13000	VLBAR .05020 .05090 .05310
			OA160	(V41F-28A)	(BS6C9F	7M7N28) (WI II	6E26) (V8R5)		(RVA00	8) (25 001	75)
	REFERENCE	E DATA '							PARAMETRIC	DATA	
SREF = LREF = BREF = SCALE =	2690.0000 SQ.F 474.8000 INCF 936.7000 INCF .0100	HES YMRP	.00	000 IN. XO 000 IN. YO 000 IN. ZO				ALPHA # PHI # BDFLAP = SPOBRK #	30.000 180.000 .000 .000	BETA # ELEVON # RUDDER #	.000 .000 .000
		RUN NO.	5012/ 0								
MACH 18.200 18.200 18.300 18 600	TIME 60.000 70.000 80.000 90.000	RN/L .26000 .26000 .25000 .27000	CN .75800 .76500 .76400 .75400	CAB - 00074 - 00075 00074 00071	CAF .10700 .11100 .11300 .11100	CLM 01630 01780 02080 02220	XCP/L .65800 .65900 .66000 .66100	CL .60300 .60700 .60500 .59800	CD .47100 .47800 .48000 .47300	L/D 1.28000 1.27000 1.26000 1.26000	VLBAR .02890 .02880 .03010 .02990
			0A160). (V41F-28A)	(B26C9F	7M7N28) (W11	6E26) (V8R5)		(RVA00	9) (25 00	r 75)
	REFERENCE	E DATA				•			PARAMETRIC	DATA	
SREF = LREF = BREF = SCALE =	2690.0000 SQ.I 474.8000 INCI 936.7000 INCI .0100	HES YMRP	= .00	000 IN. XO 000 IN. YO 000 IN. ZO				ALPHA = PH1 = BDFLAP = SPDBRK =	30.000 180.000 .000,	BETA = ELEVON = RUDDER =	.000 .000 .000
		RUN NO.	5000/ 0								
MACH 17.900 18.000 18.100 18.300	80.000 90.000	RN/L .34000 .35000 .35000 .35000	CN .77400 .77200 .76400 .76000	CAB 00074 00072 00071 00076	CAF .10500 .10600 .10600 .10700	CLM 02540 01980 01940 01820	XCP/L .66200 .65900 .65900	CL .61800 .61600 .60900 .60500	CD .47800 .47800 .47400 .47200	L/D 1.29000 1.29000 1.29000	VLBAR .02510 .02500 .02560 .02580

OA160 (VM15=28A) (B2BCGF7M7N2B)(W116F2B)(VBR5) (RVA004) (25 OCT 75)

			OA160	. (V41F-28A)	(B26C9F	7M7N28) (W116	SE26) (V8R5)		(RVA00	4) (25 OCT	75)
	REFERENC	E DATA							PARAMETRIC	DATA	
SREF = LREF = BREF = SCALE =	2690.0000 SQ. 474.8000 INC 936.7000 INC	HES YMRP	= .00	00 IN. XO 00 IN. YO 00 IN. ZO				ALPHA = PHI = BDFLAP = SPDBRK =	30.000 .000 .000	BETA = ELEVON = RUDDER =	.000 .000 .000
		RUN NO.	5001/ 0				ř				
MACH 18.300 18.300	TIME 90.000 100.000	RN/L .32000 .28000	CN .75600 .75100	CAB 00080 00082	CAF .11000 .10900	CLM 02150 01910	XCP/L .66000 .65900	CL ,60000 .59600	CD .47300 .47000	L/D 1.27000 1.27000	VLBAR .02650 .02550
			0A160	(V41F-28A)	(B26C9F	7M7N28) (W118	5E26)(V8R5)		(RVA00	5) (25 OCT	75 J
	REFERENC	E DATA							PARAMETRIC	DATA	
SREF = LREF = BREF = SCALE =	2690.0000 SQ. 474.8060 INC 936.7000 INC .0100	HES YMRP	× .00	00 IN. XO 00 IN. YO 00 IN. ZO				ALPHA = PHI = BDFLAP = SPOBRK =	30.000 .000 .000	BETA = ELEVON = RUDDER =	.000 .000 .000
		RUN NO.	5004/ 0								
MACH 18.700 18.600 18.600 18.700	FIME 70.000 80 000 90.000 100.000	RN/L .47000 .43000 .43000 .38000	CN .79700 .78300 .77300 .76300	CAB 00098 - 00099 - 00097 00093	CAF .10200 .10200 .10100 .09990	CLM 02290 02060 01850 - 01740	XCP/L .66100 .66000 .65900 .65800	CL .63900 .62700 .61900 .61100	CD .48700 .48000 .47400 .46800	L/D 1.31000 1.31000 1.31000 1.31000	VLBAR .02290 .02380 .02400 .02540
			OA 160	(V41F-28A)	(B26C9F	7M7N28) (W116	5E26) (V8R5)		(RVA00	6) (25 001	75)
	REFERENC	E DATA							PARAMETRIC	DATA	
SREF = LREF = BREF = SCALE =	2690.0000 SQ. 474.8000 INC 936.7000 INC	HES YMRP	= .00	000 IN. XO 000 IN. YO 000 IN. ZO				ALPHA = PHI = BOFLAP = SPOBRK =	30.000 180.000 .000 .000	BETA = ELEVON = RUDDER =	.000 .000 .000
		RUN NO.	5006/ 0								
MACH 18.500 18.900 19.300	TIME 60.000 70.000 80:000	RN/L .11000 .10000 .10000	CN .83800 .85200 .86600	CAB 00106 0018 00132	CAF .14700 .15400 .16100	CLM 03490 03890 04190	XCP/L .66500 .66700 .66800	CL .65200 .65100 .66900	CD .54600 .56000 .57300	L/D 1.19000 1.18000 1.17000	VLBAR .04580 .04670 .05090

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RUN NO. 5005/ 0

CN .84100 .84700

.84300

RN/L .12000 .13000 .14000

MACH 18.300 18.800 19.000

TiME 60.000 70.000 80.000

DATE 09 DEC 75	区 24	-	OA16	SO TABULAT	ED SOURCE DA	TA			PAGE	1
v		OA160,	(V41F-28A)	(B26C9F7	M7N28) (W116E	(26) (VBR5)		(RVA00	1) (25 OCT	75)
REFE	RENCE DATA							PARAMETRIC	DATA	
SREF = 2690.0000 LREF = 474.8000 BREF = 936.7000 SCALE = .0100		= 1076.7000 = .0000 = 375.0000	IN. YO	-	ì		ALPHA = PHI = BDFLAP = SPDBRK =	30.000 .000 .000	BETA = ELEVON = RUDDER =	.000 .000 .000
	RUN NO	. 5003/ 0								
MACH TIME 20.300 110.00	RN/L 0 .08000		CAB .00183	CAF .17900	CLM 02890	XCP/L .66400	CL .58300	CD .54300	L/D 1.07000	VLBAR .05810
		OA160.	(V41F-28A)	(B26C9F7	M7N28) (WI 16E	(26) (V8R5)		(RVADO	2) (25 OCT	75 }
REFE	RENCE DATA							PARAMETRIC	DATA	
SREF = 2590.0000 LREF = 474.8000 BREF = 936.7000 SCALE = .0100	INCHES YMRP	= 1076.7000 = .0000 = 375.0000	IN. YO				ALPHA # PHI # BDFLAP # SPDBRK #	30.000 .000 .000	BETA # ELEYON = RUDDER #	.000 .000 .000
	RUN NO	. 4998/ 0								
MACH TIME 20.000 84.00 20.500 94.00 20.800 104.00	0 .11000	.85700 - 85600 -	CAB 00135 .00153 .00143	CAF .14700 .15200 .15300	CLM 03690 03710 03190	XCP/L .66600 .66600 .66400	CL .66900 .66600 .65100	CD .55600 .55900 .55300	L/D 1.20000 1.19000 1.18000	VLBAR .04640 .05000 .05010
		QA160,	(V41F-28A)	(B26C9F7	M7N28) (WI 16E	(26) (V8R5)		(RVADO	3) (25 OCT	75)
REFE	RENCE DATA							PARAMETRIC	DATA	
SREF = 2690.0000 LREF = 474.8000 BREF = 936.7000 SCALE = .0100	INCHES YMRP	= 1076.7000 = .0000 = 375.0000	IN. YO				ALPHA = PHI = BDFLAP % SPDBRK =	30.000 .000 .000	BETA = ELEVON = RUDDER =	.000 .000 .000

CAF .15100 .14700 .14300

CLM -.03960 -.03560

-.03130

XCP/L .66700 .66500 .66400

CL .65300

.66000

.65900

CAB -.00113 -.00107 -.00105

CD .55100 .55100

.54500

VLBAR .04320 .04270 .04300

L/D 1.18000 1.20000 1.21000

APPENDIX

TABULATED SOURCE DATA

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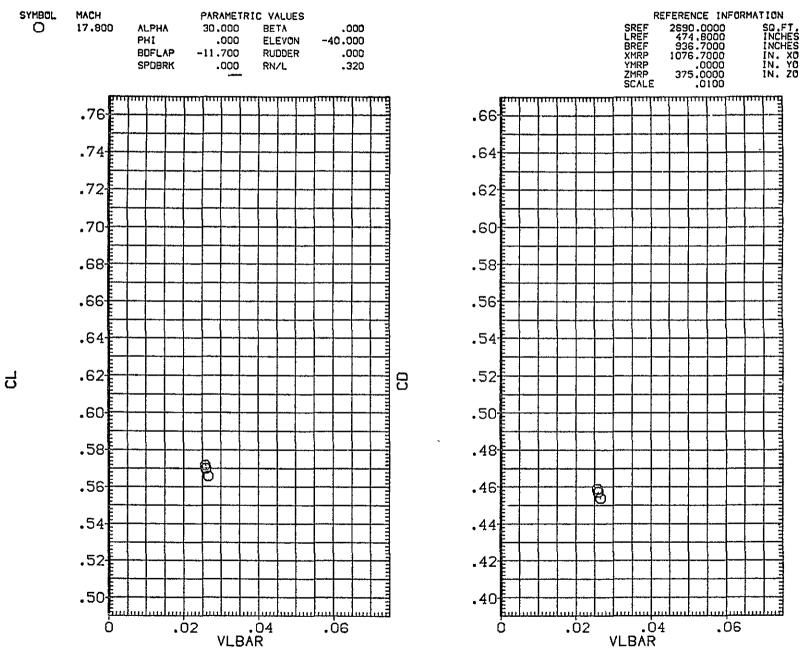


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

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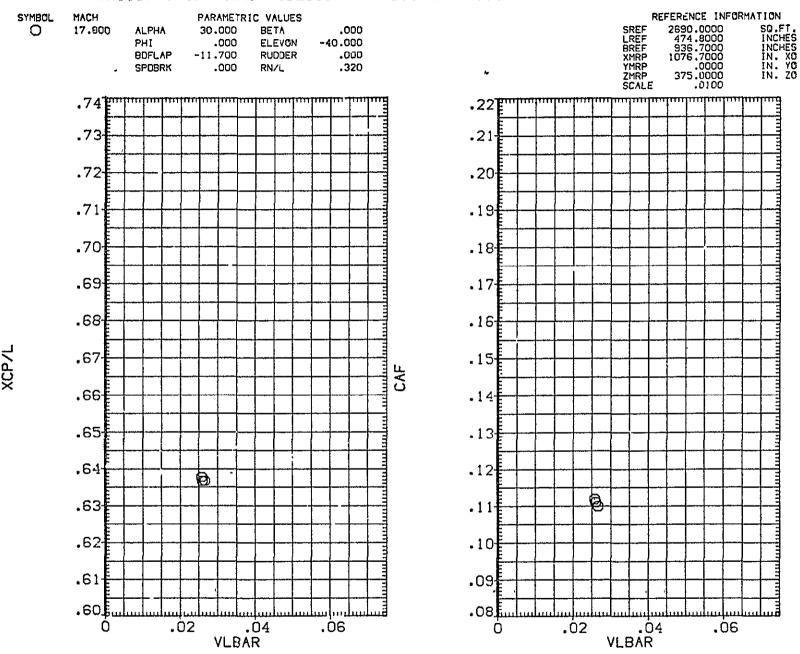


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

PAGE

OA160, (V41F-28A) (626C9F7M7N28)(W116E26)(V8R5)(AVA014)

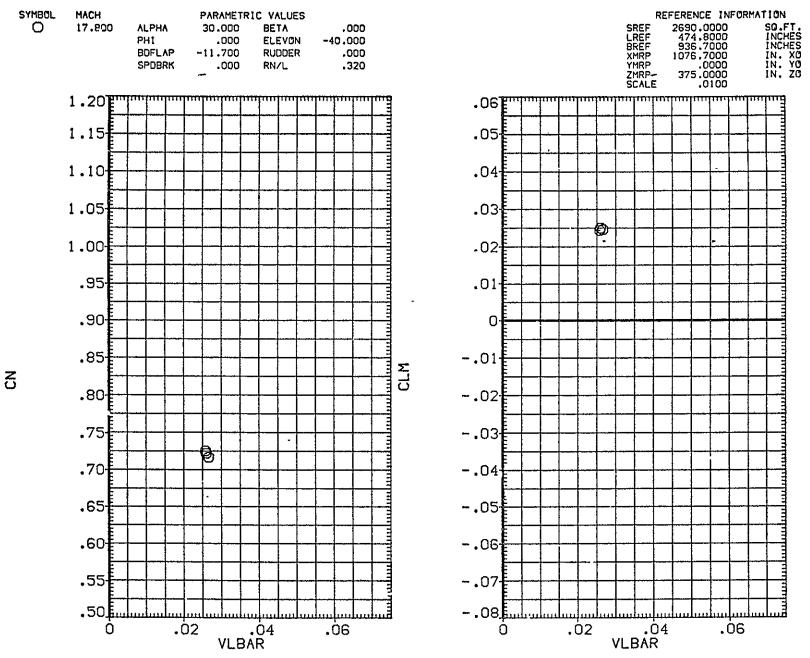


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

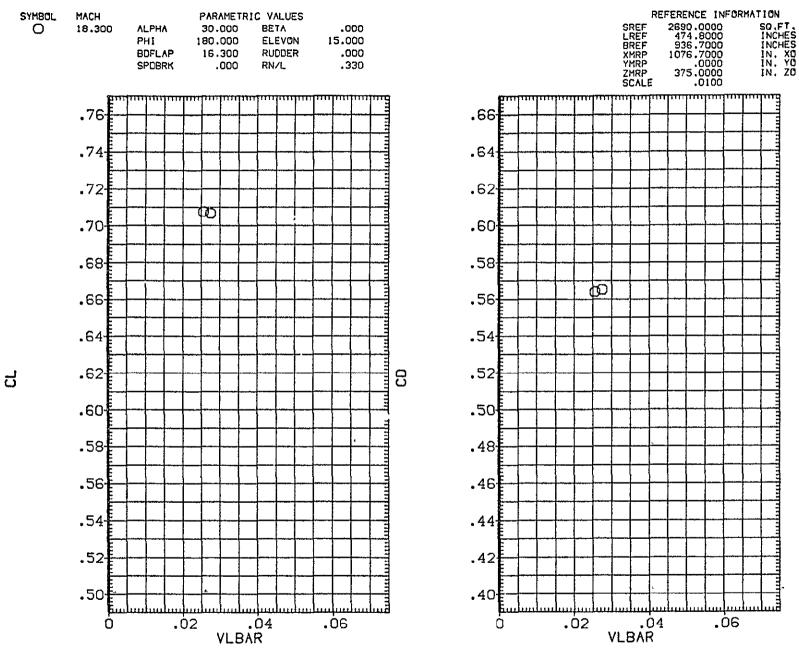


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

PAGE

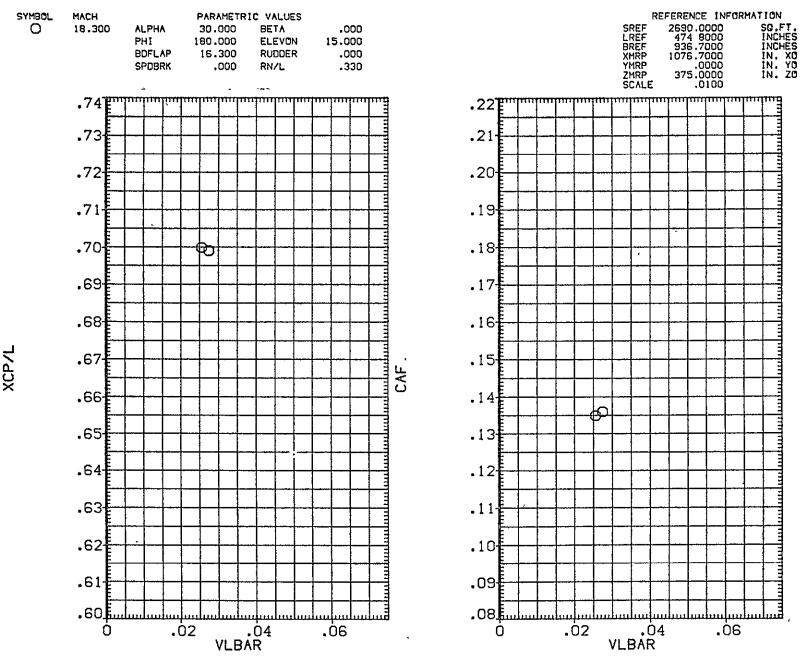


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

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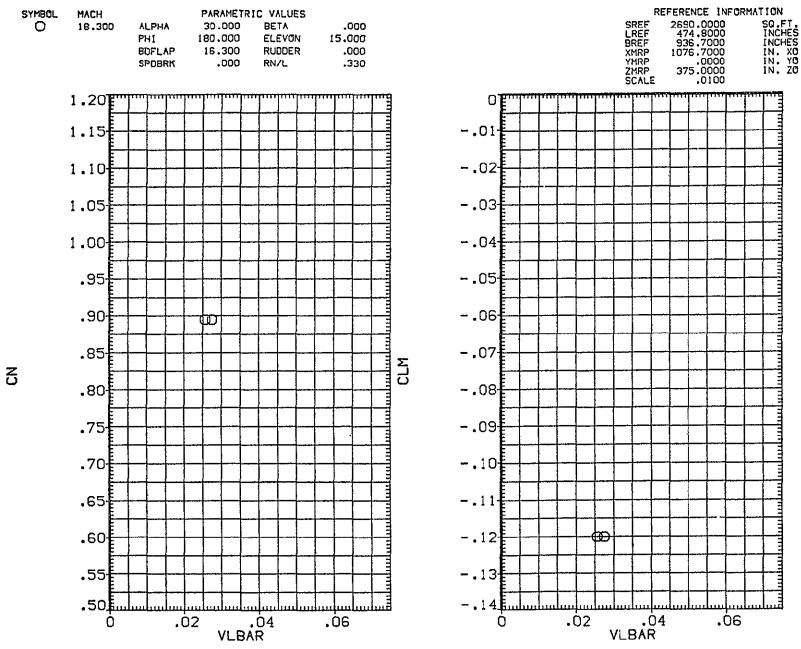


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

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ØA160, (V41F-28A) (B26C9F7M7N28)(W116E26)(V8R5)(AVA012)

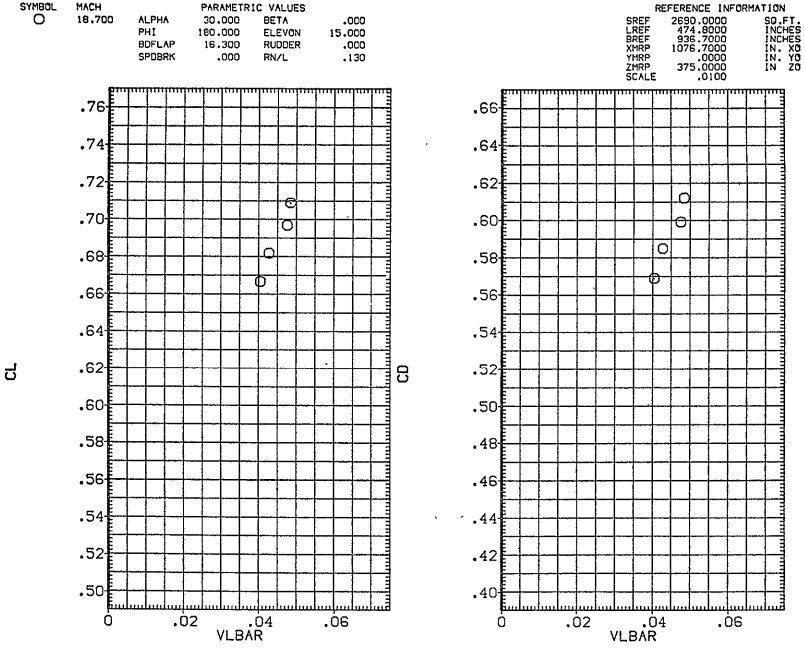


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

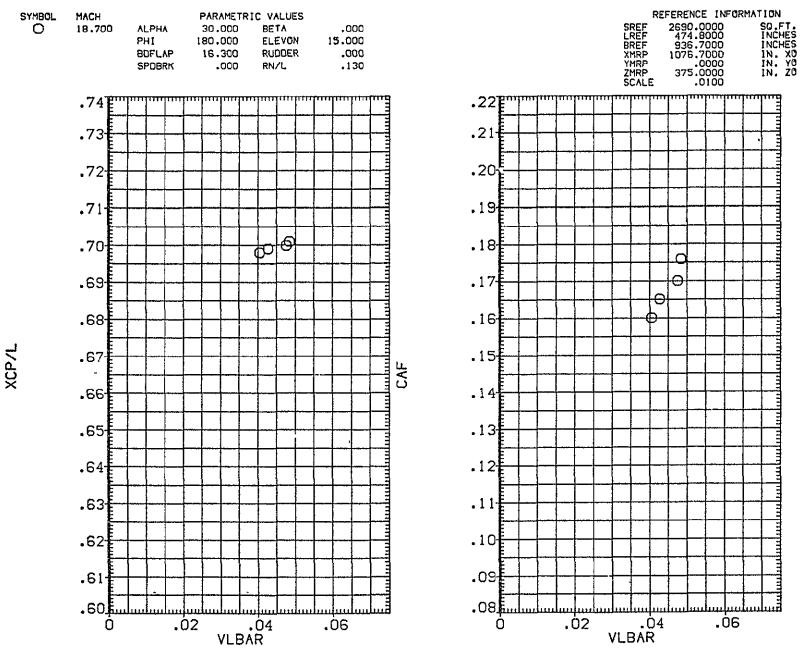


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

ØA160, (V41F-28A) (B26C9F7M7N28)(W116E26)(V8R5)(AVA012)

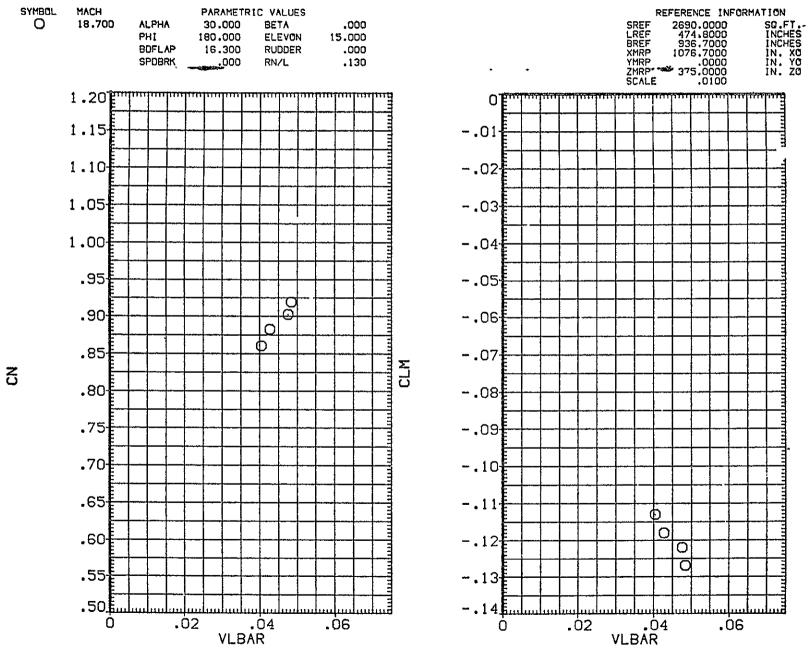


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

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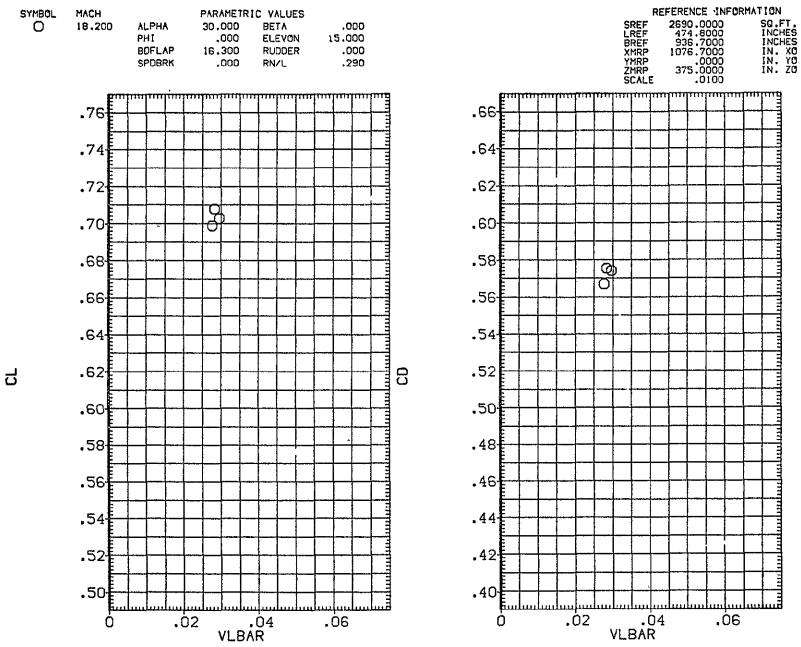


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

OA160, (V41F-28A) (B26C0F7M7N28)(W116E26)(V8R5)(AVA011)

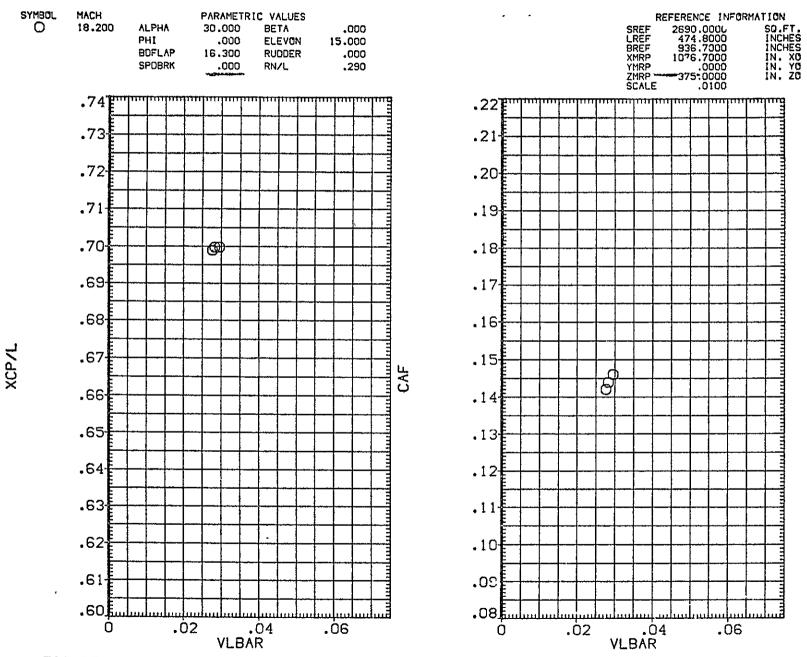


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

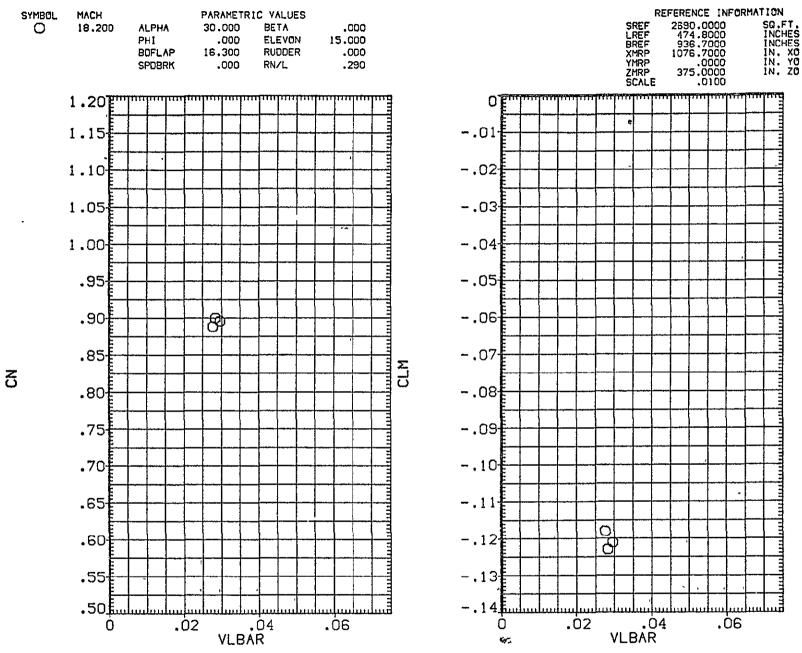


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

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OA160, (V41F-28A) (B26C9F7M7N28)(W116E26)(V8R5)(AVA010)

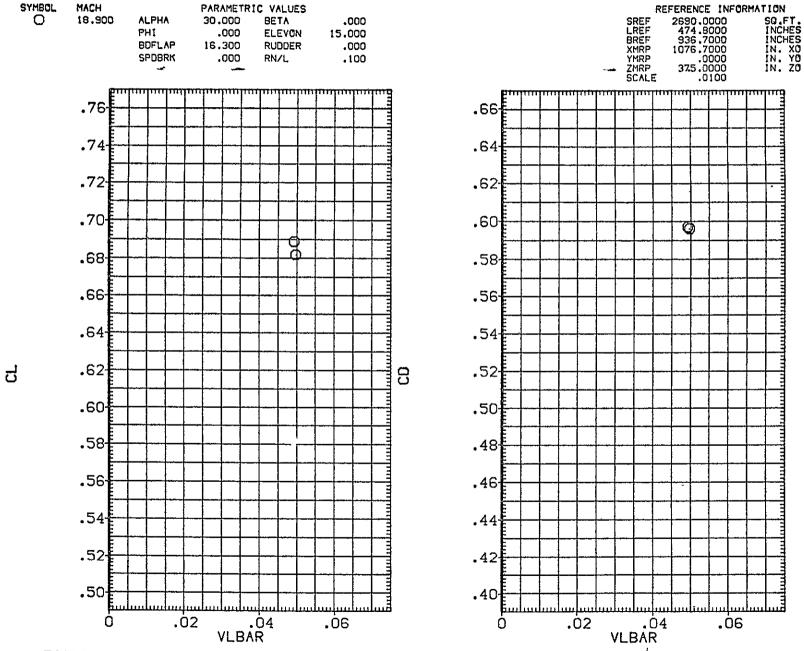


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

PAGE

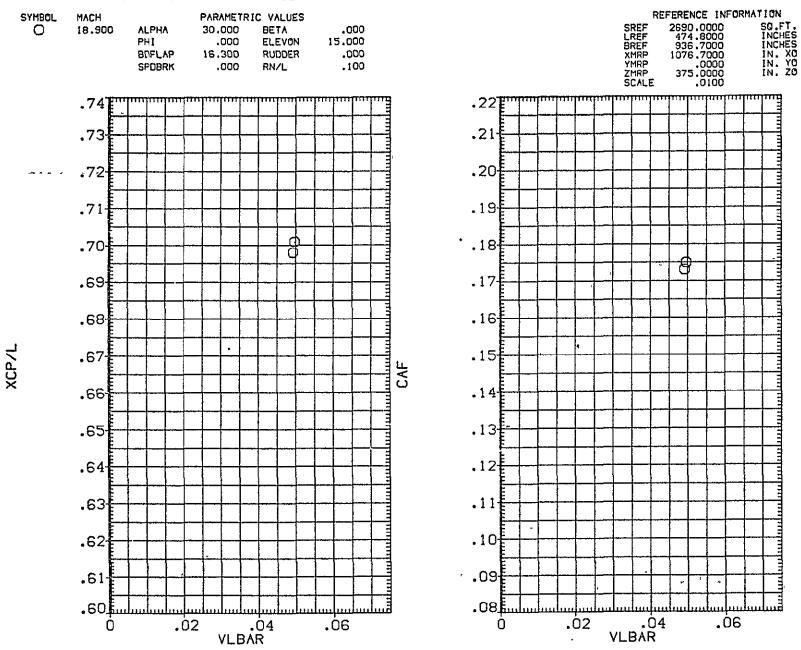


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

0A160, (V41F-28A) (B26C9F7M7N28)(W116E26)(V8R5)(AVA010)

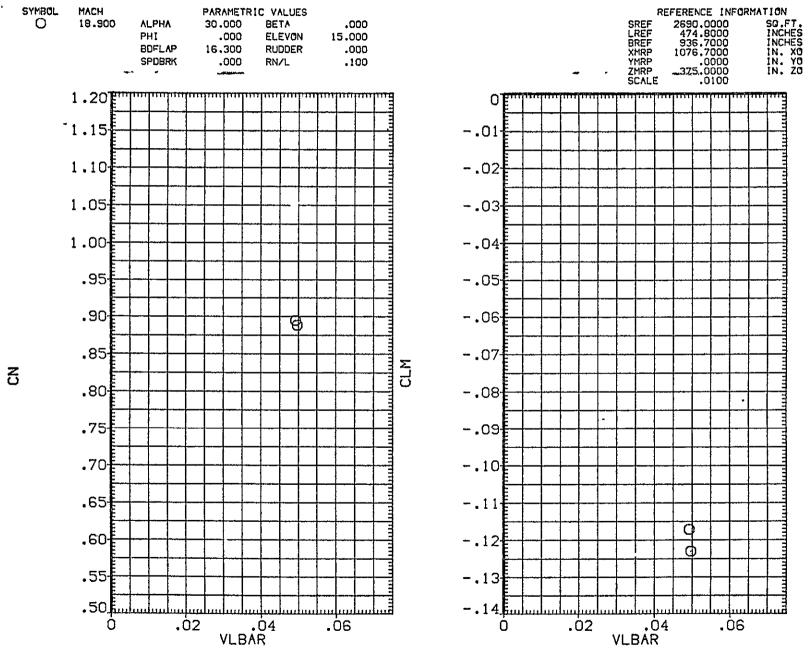


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

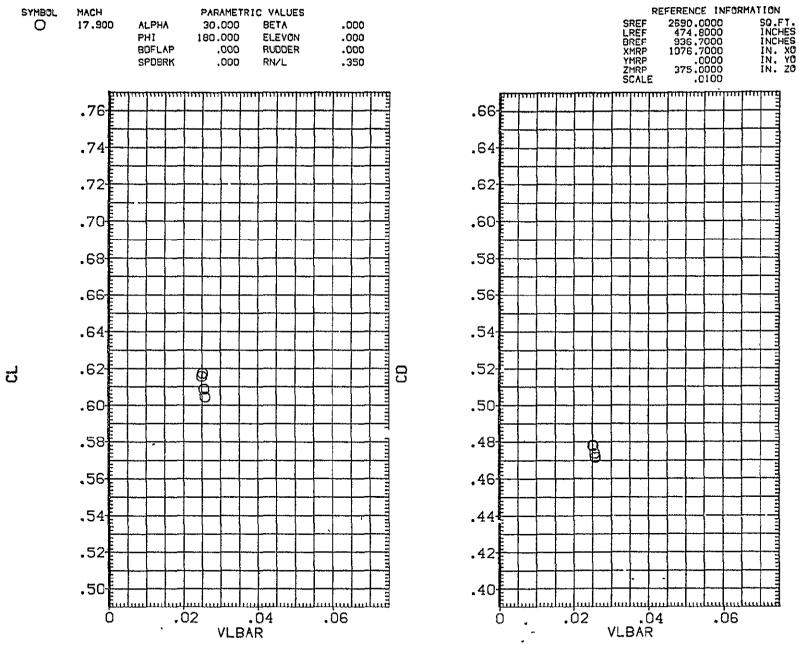


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

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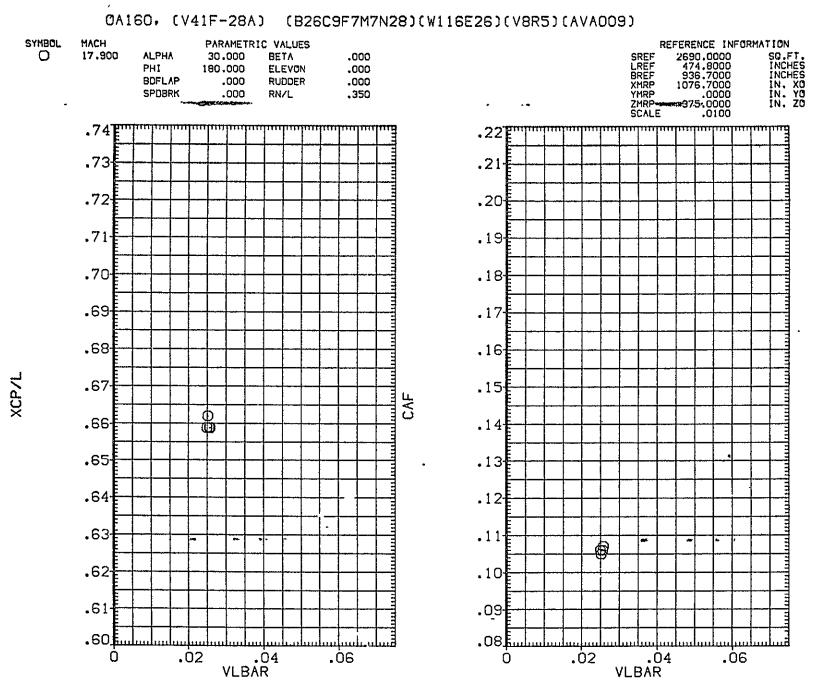


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

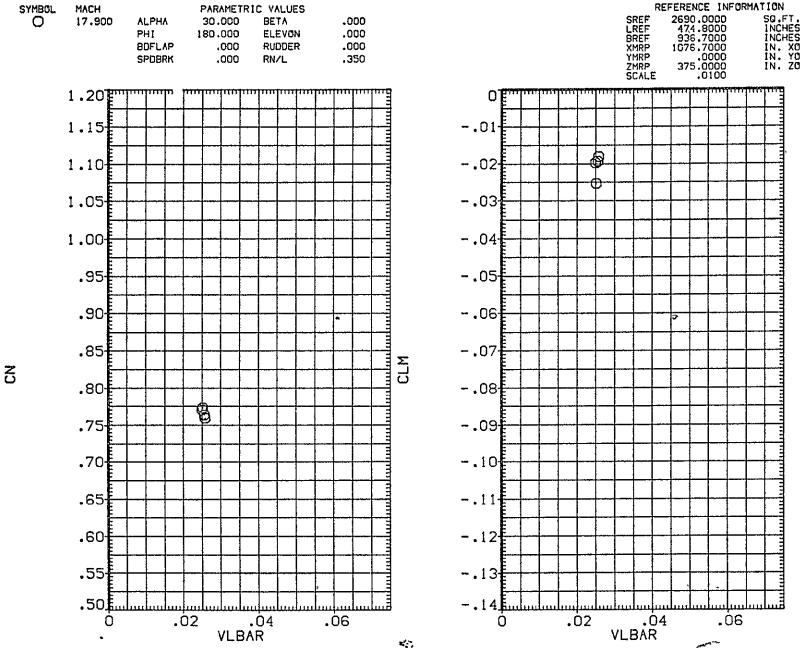


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B-PAGE

0A160, (V41F-28A) (B26C9F7M7N28)(W116E26)(V8R5)(AVA008)

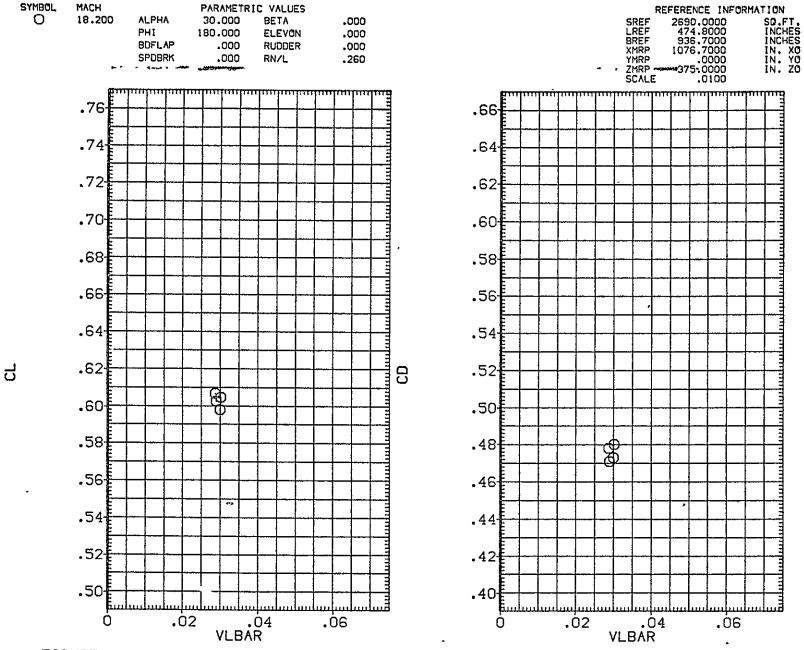


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

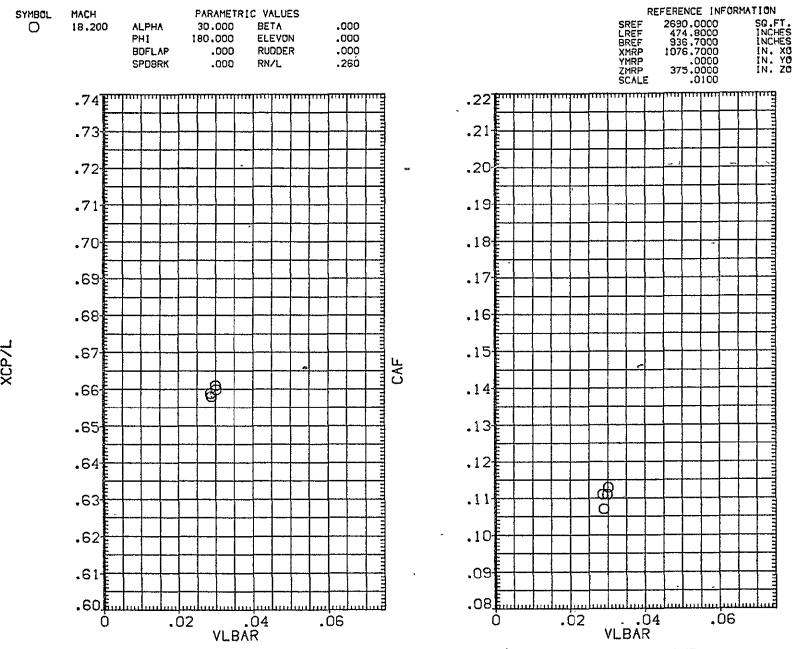


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

0A160, (V41F-28A) (B26C9F7M7N28)(W116E26)(V8R5)(AVA008)

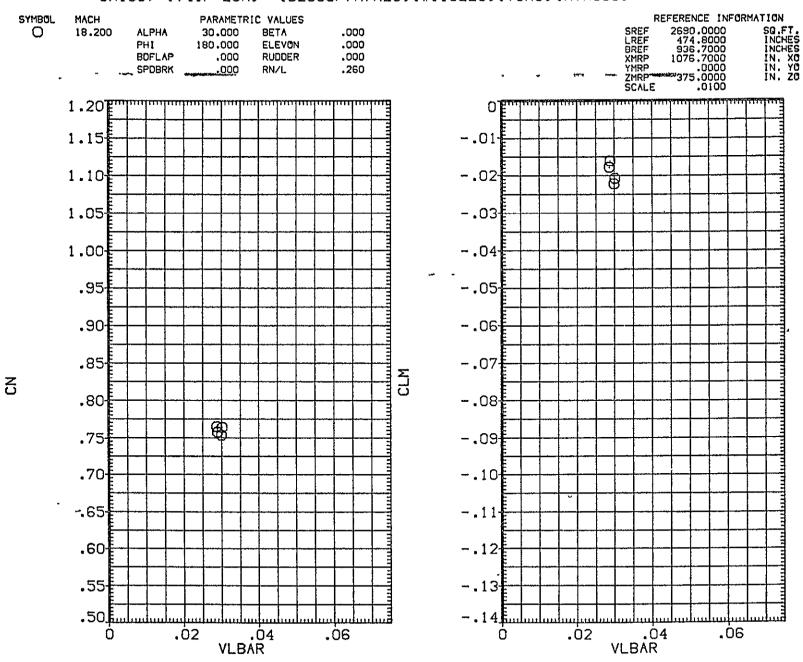


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

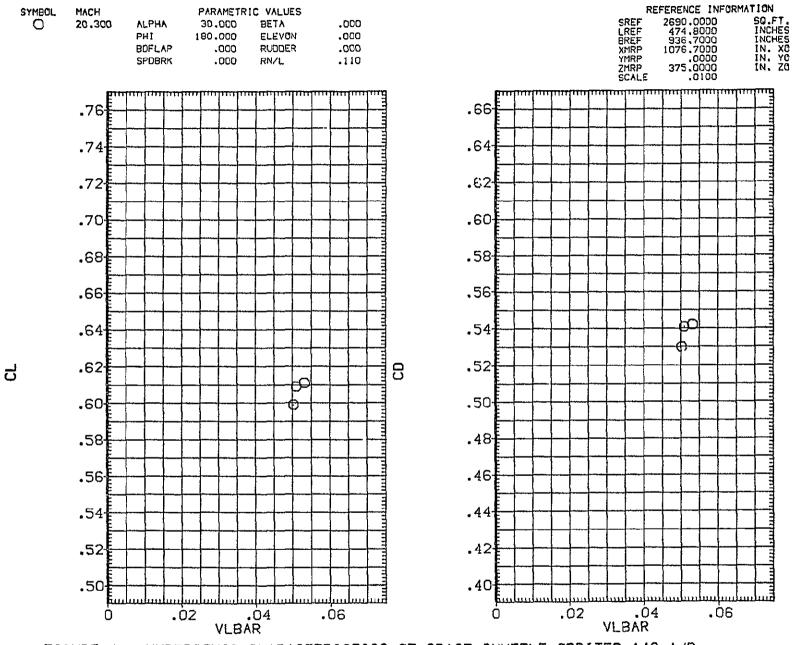


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

0A160, (V41F-28A) (B26C9F7M7N28)(W116E26)(V8R5)(AVA007)

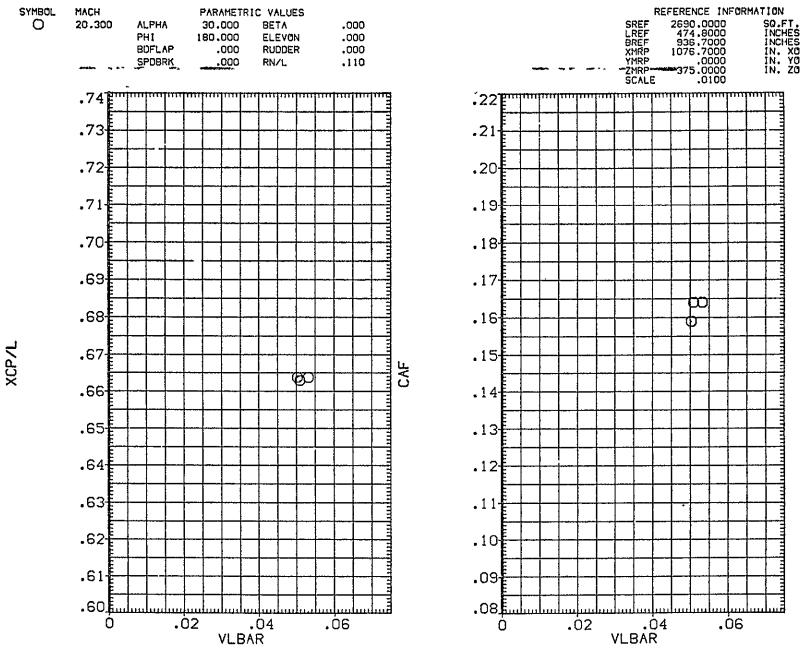
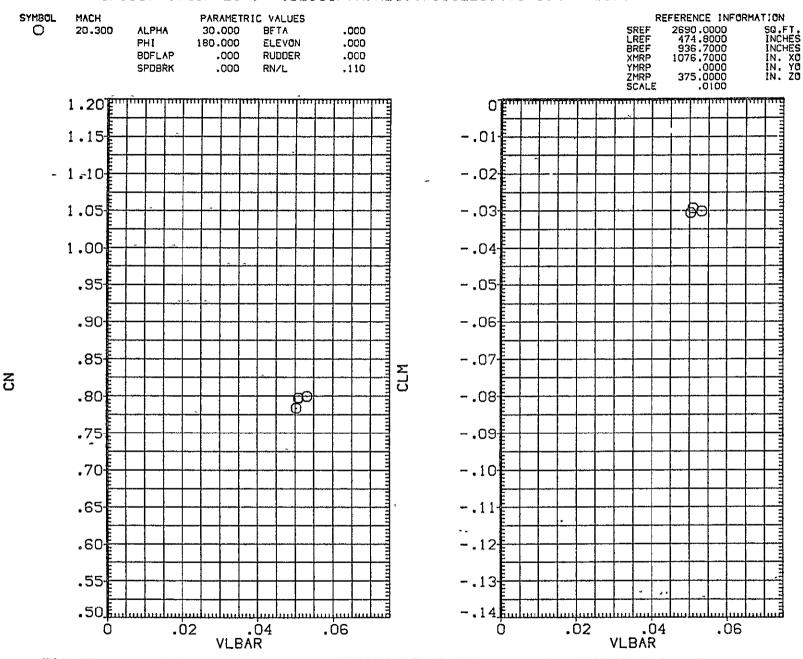


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B



HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

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VLBAR

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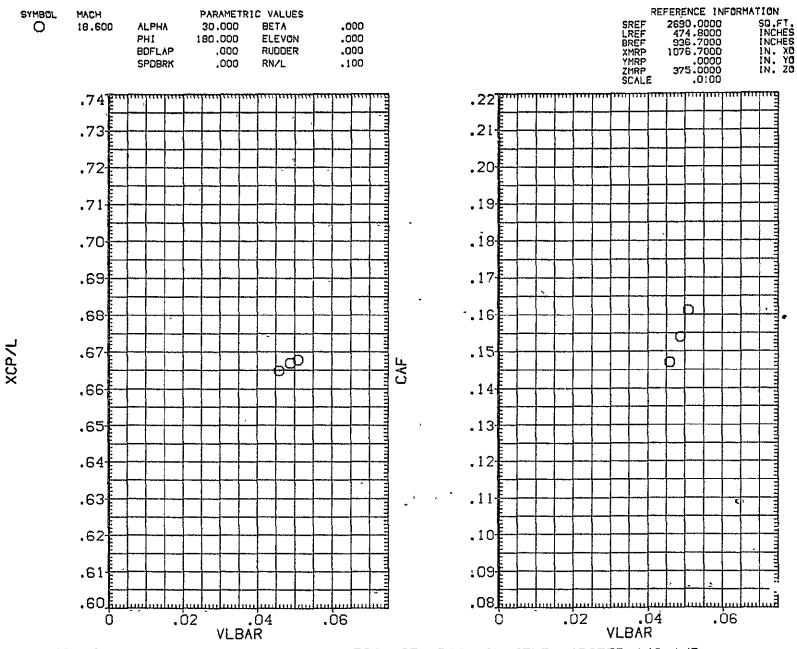


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

0A160. (V41F-28À) (B26C9F7M7N28)(W116E26)(V8R5)(AVA006)

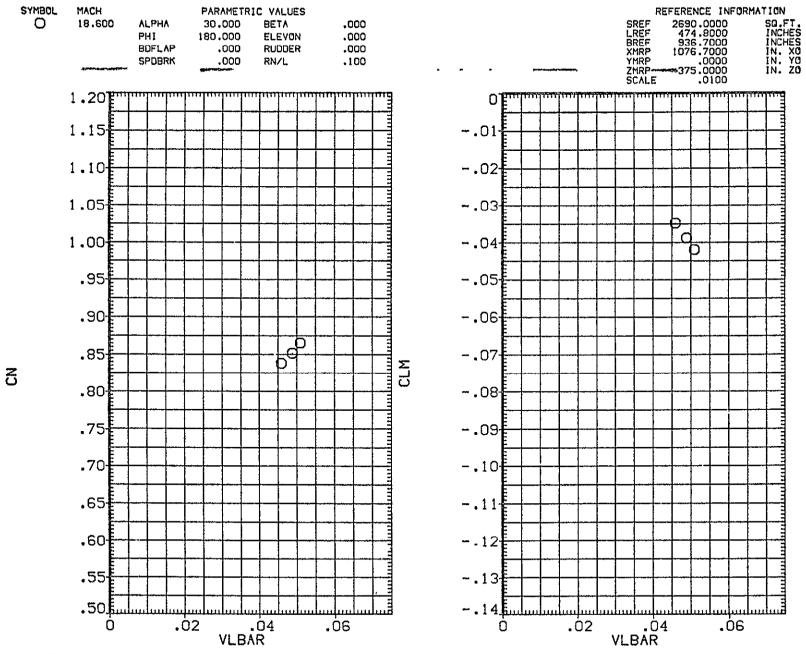


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

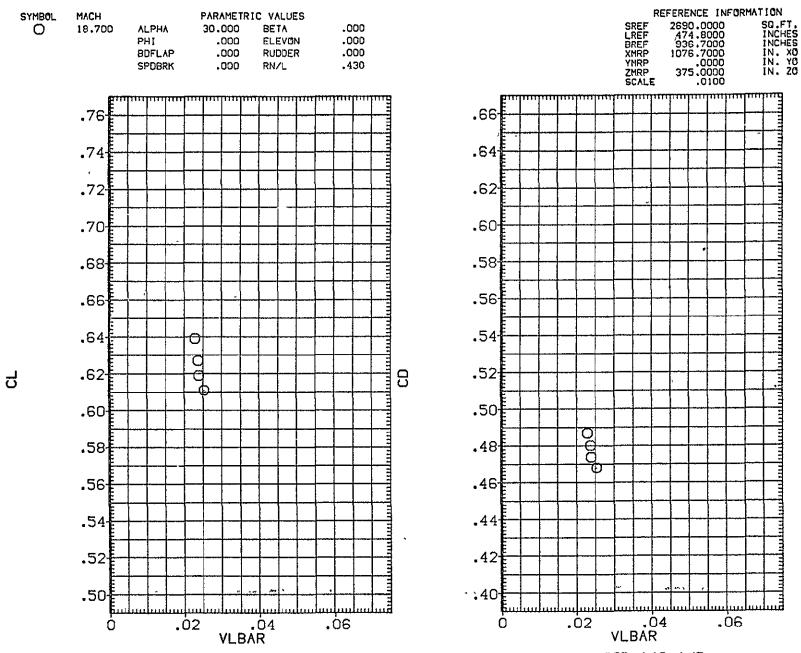


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

OA160, (V41F-28A) (B26C9F7M7N28)(W116E26)(V8R5)(AVA005)

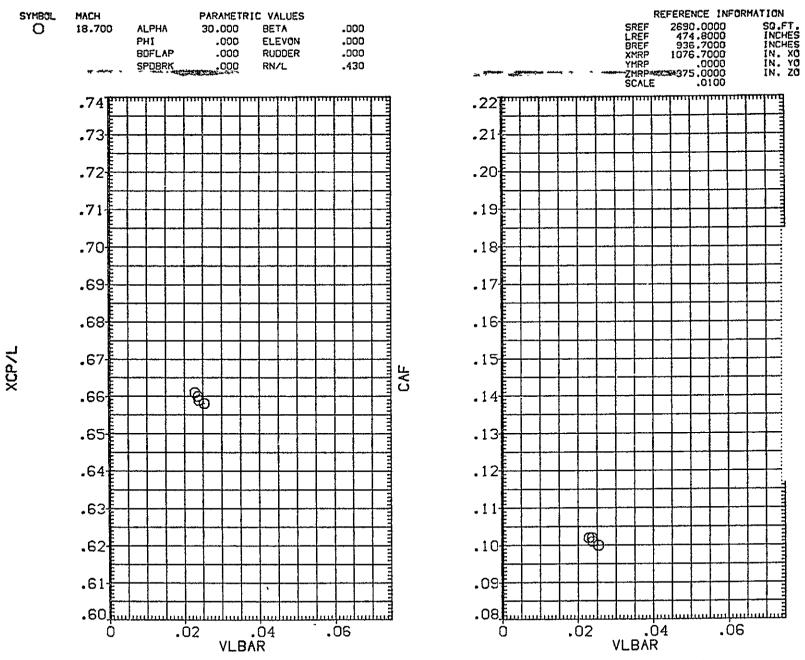


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

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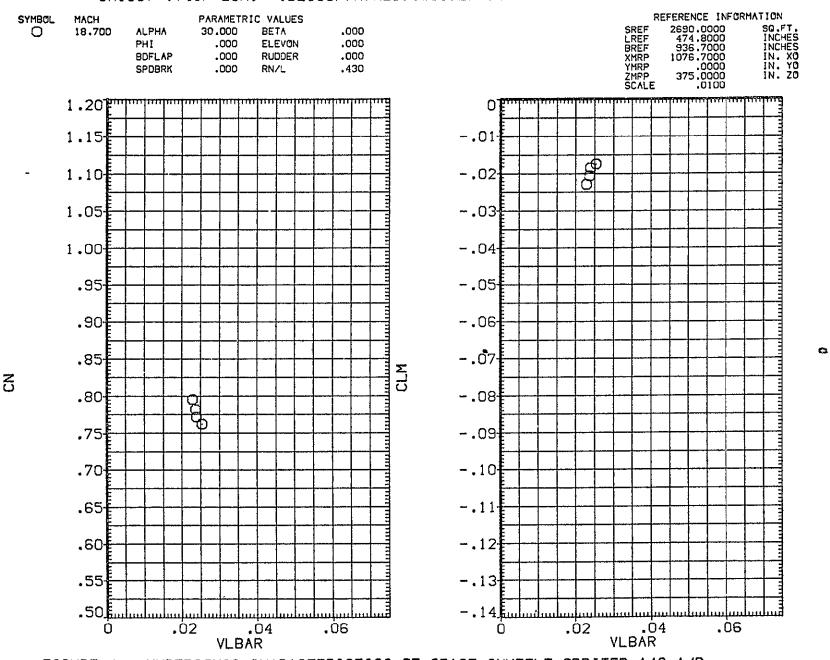


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

0A160, (V41F-28A) (B26C9F7M7N28)(W116E26)(V8R5)(AVA004)

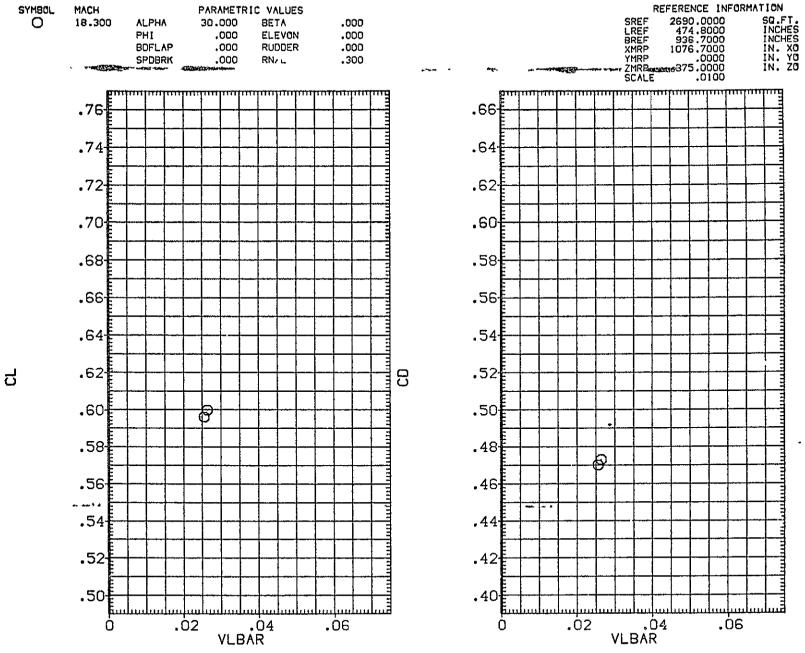


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

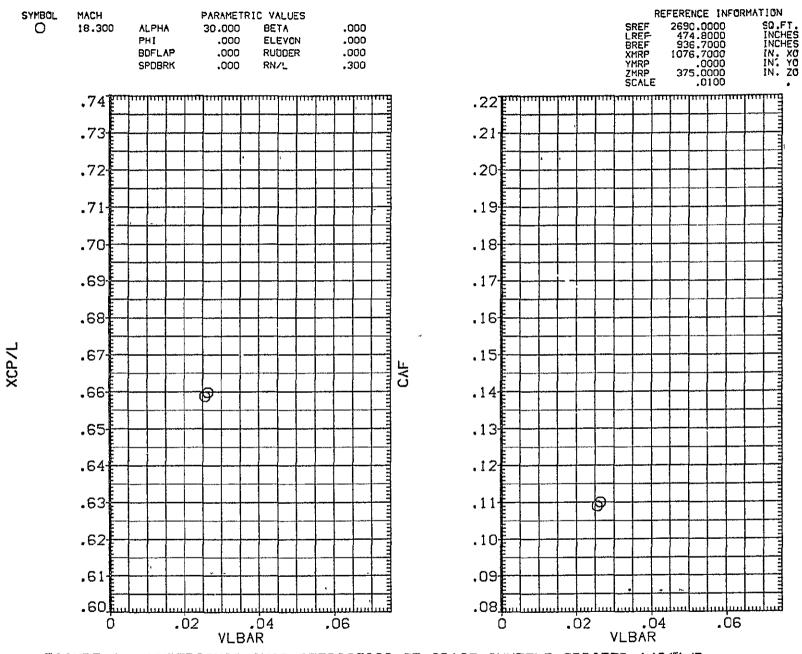


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140-74/B

0A160, (V41F-28A) (B26C9F7M7N28)(W116E26)(V8R5)(AVA004)

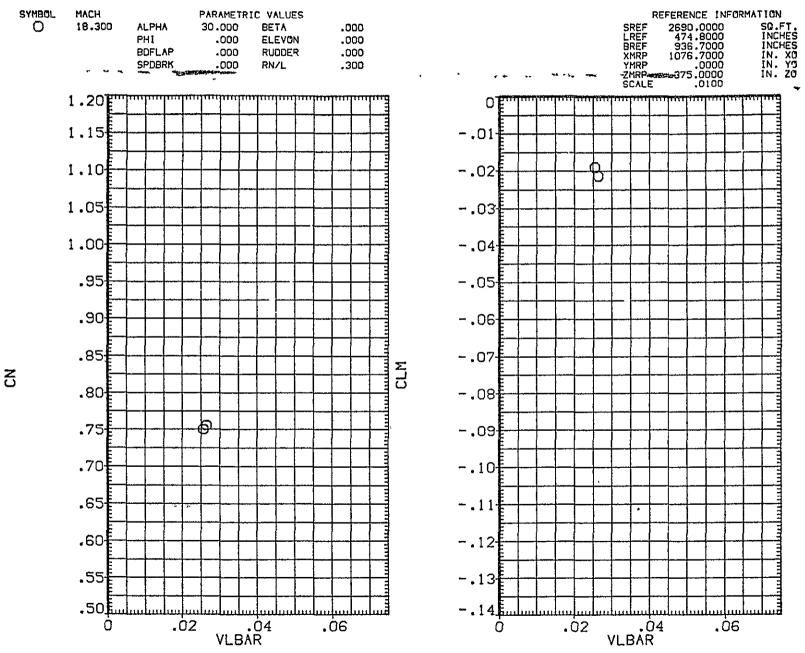


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

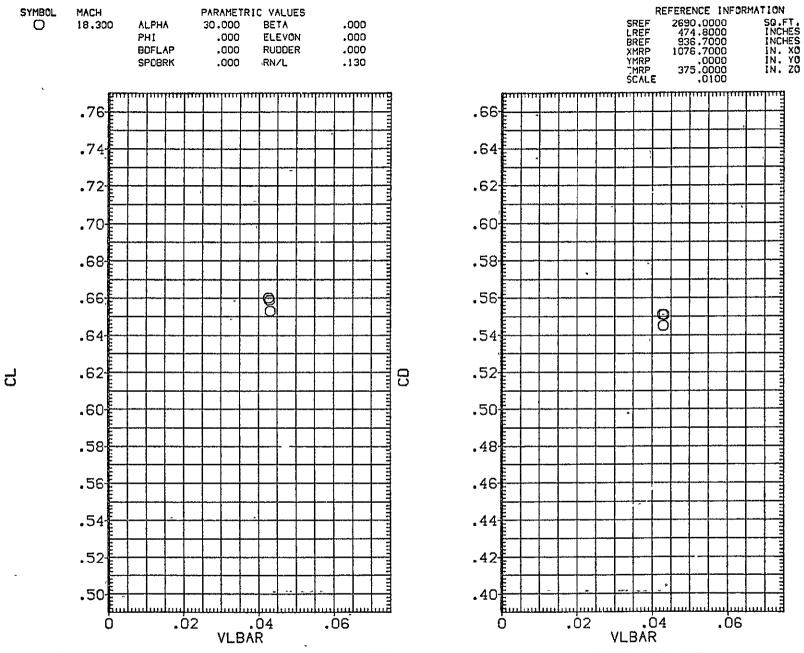
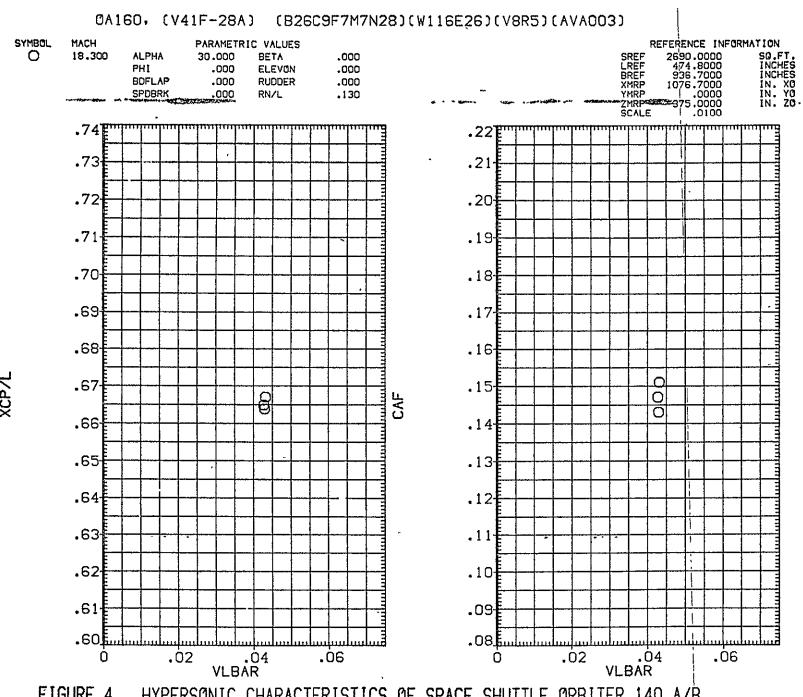


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

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HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B FIGURE 4.

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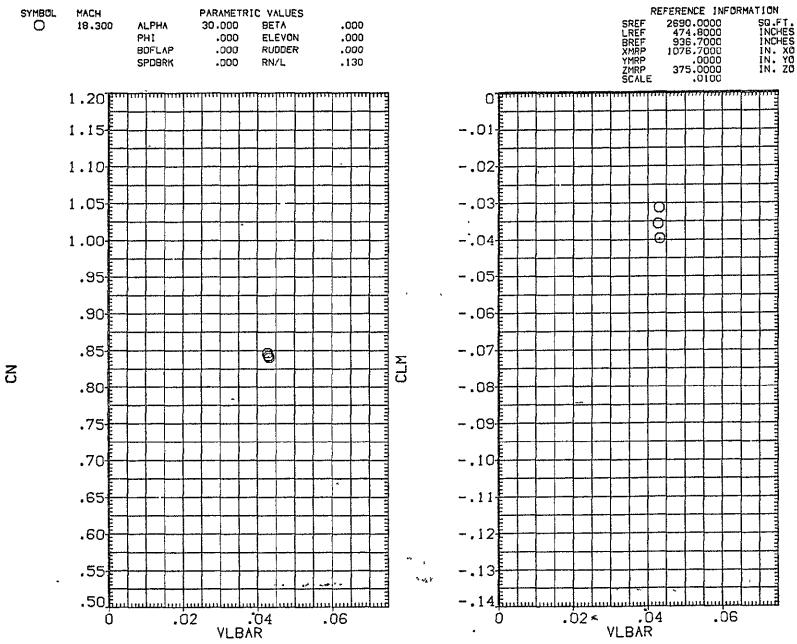


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

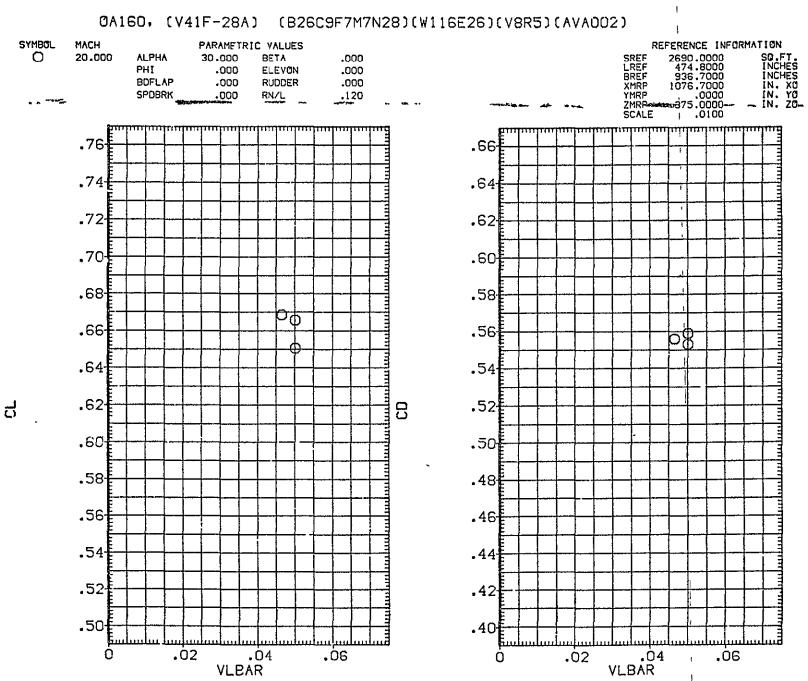


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

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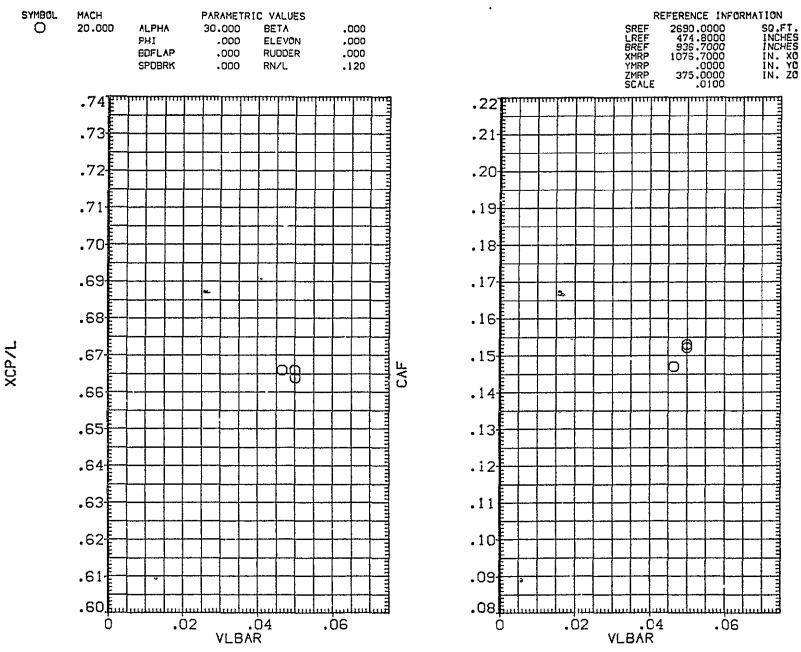


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

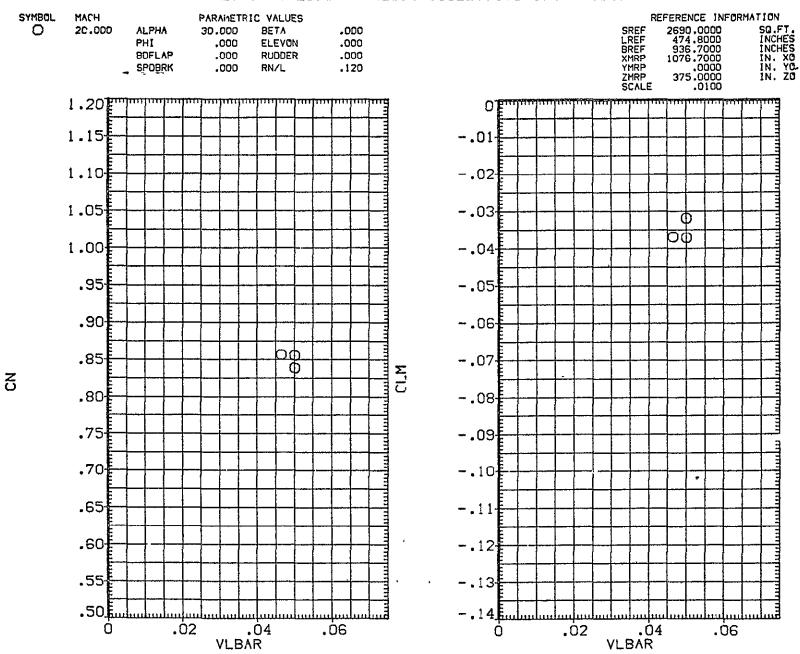


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

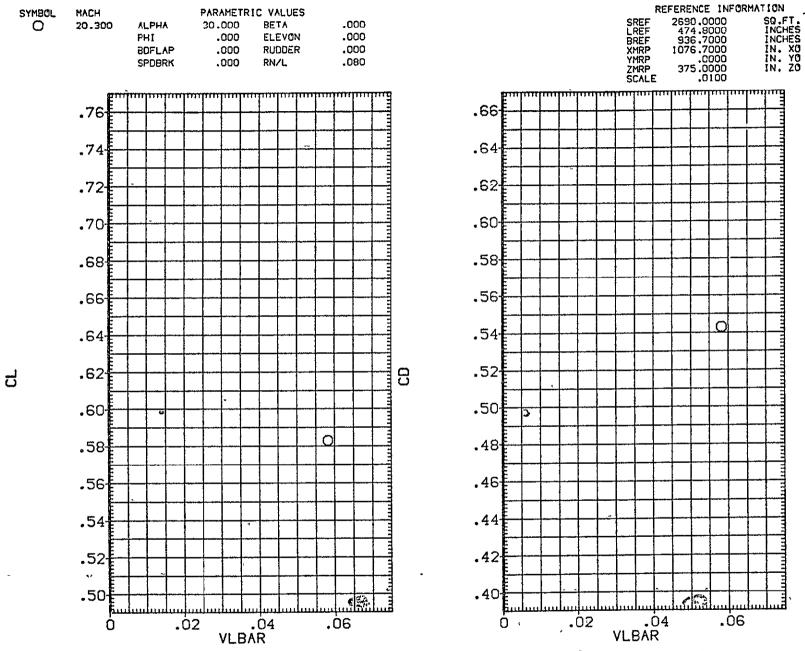


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B

0A160, (V41F-28A) (B26C9F7M7N28)(W116E26)(V8R5)(AVA001)

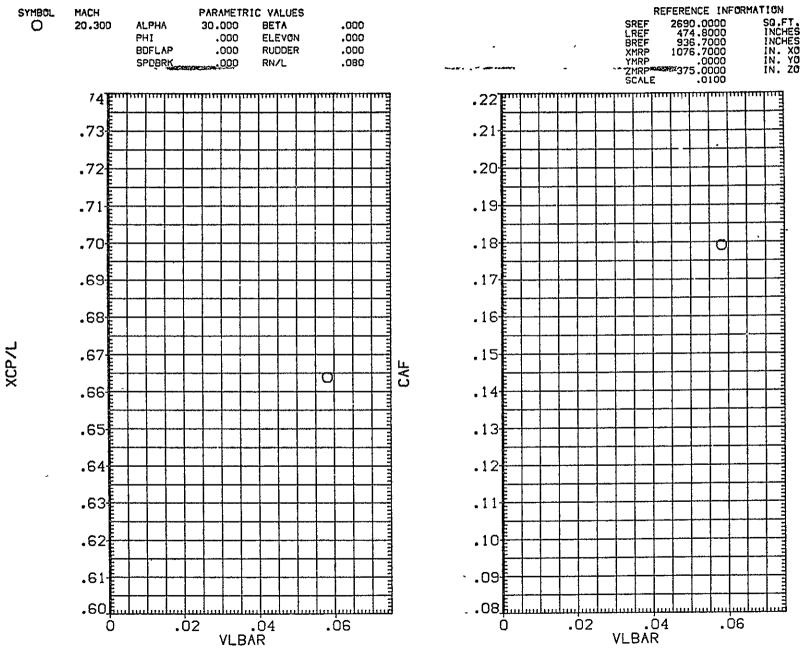


FIGURE 4. HYPERSONIC CHARACTERISTICS OF SPACE SHUTTLE ORBITER 140 A/B